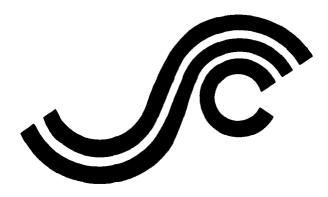




# SL-7 EXTREME STRESS DATA COLLECTION AND REDUCTION





This document has been approved for public release and sale; its distribution is unlimited.

# SHIP STRUCTURE COMMITTEE

1981

82 07 19 172

#### SHIP STRUCTURE CONNITTEE

The SNIP STRUCTURE COMMITTEE is constituted to prosecute a research program to improve the hull structures of ships and other marine structures by an extension of knowledge pertaining to design, materials and methods of construction.

RAdm Clyde T. Lush, Jr. (Chairman) Chief, Office of Merchant Marine Safety U. B. Coast Guard Needquarters

Mr. P. M. Pelermo Executive Director Ship Design & Integration Directorate Naval Sea Systems Command

Nr. W. N. Mannan Vice President American Bureau of Shipping Mr. J. Gross
Deputy Assistant Administrator for
Commercial Development
Maritime Administration

Mr. J. B. Gregory Chief, Research & Development Staff of Planning & Assessment U.S. Geological Survey

Mr. Thomas W. Allen Chief Engineering Officer Military Sealift Command

LCdr D. B. Anderson, U.S. Coast Guard (Secretary)

#### SHIP STRUCTURE SUBCONCUTTER

The SHIP STRUCTURE SUBCONNITTEE acts for the Ship Structure Committee on technical matters by providing technical coordination for the determination of goals and objectives of the program, and by evaluating and interpreting the results in terms of structural design, construction and operation.

U. S. CUAST GUARD

Capt. R. L. Brown Cdr. J. C. Card Mr. R. E. Williams Cdr. J. A. Sanial

Mr. R. Chiu

HILTARY SEALIFY CONNAND

Nr. Albert Attermeyer Nr. T. W. Chapman Nr. A. B. Stavovy Nr. D. Stein

NAVAL SEA SYSTEMS COMMAND

Nr. J. B. O'Brien Nr. W. C. Sandberg Ledr D. W. Whiddon Nr. T. Nemura (Contracts Admin.)

MARITIME ADMINISTRATION

Hr. N. O. Haumer Dr. W. H. Maclean Hr. F. Seibold Hr. M. Touma

NATIONAL ACADEMY OF SCIENCES SHIP RESEARCH CONNITTEE

Mr. A. Dudley Haff - Liaison Mr. R. V. Rumbe - Liaison

SOCIETY OF NAVAL ARCHITECTS & MARINE ENGINEERS

Mr. A. B. Stavovy - Liaison

WELDING RESEARCH COUNCIL

Mr. K. M. Koopman - Linison

AMERICAN BUREAU OF SHIPPING

Dr. D. Liu Nr. I. L. Stern

U. S. GEOLOGICAL SURVEY

Mr. R. Giangerelli Mr. Charles Smith

INTERNATIONAL SHIP STRUCTURES CONGRESS

Mr. S. G. Stiansen - Limon

AMERICAN IRON & STEEL INSTITUTE

Mr. R. H. Sterne - Limon

STATE UNIV. OF NEW YORK MARITIME COLLEGE Dr. W. R. Porter - Lisison

U. S. COAST GLARD ACADEMY LCdr R. G. Vorthman - Limison

U. S. NAVAL ACADEMY

Dr. R. Battacharvya - Liaison

U. S. MERCHANI MARINE ACAMEMI Dr. Chin-Boa Kin - Liaison Member Agencies:

United States Coast Guard Naval Sea Systems Command Military Sealift Command Maritime Administration United States Geological Survey American Bureau of Shipping



Address Correspondence to:

Secretary, Ship Struct. J Committee U.S. Coast Guard Headquarters, (G-M/TP 13) Washington, D.C. 20593

An Interagency Advisory Committee Dedicated to Improving the Structure of Ships

SR-1245

1981

This report is one of a group of Ship Structure Committee Reports which describe the SL-7 Instrumentation Program. This program, a jointly funded undertaking of Sea-Land Service, Inc., the American Bureau of Shipping and the Ship Structure Committee, represents an excellent example of cooperation between private industry, classification authority and government. The goal of the program is to advance understanding of the performance of ships' hull structures and the effectiveness of the analytical and experimental methods used in their design. While the experiments and analyses of the program are keyed to the SL-7 containership and a considerable body of the data developed relates specifically to that ship, the conclusions of the program will be completely general, and thus applicable to any surface ship structure.

The program includes measurement of hull stresses, accelerations and environmental and operating data on the S.S. Sea-Land McLean; development and installation of a microwave radar wavemeter for measuring the seaway encountered by the vessel, a wave tank model study and a theoretical hydrodynamic analysis which relate to the wave induced loads, a structural model study and a finite element structural analysis which relate to the structural reponse, and installation of long-term stress recorders on each of the eight vessels of the class. In addition, work is underway to develop the initial correlations of the results of the several program elements.

Results of each of the program elements are being made available through the National Technical Information Service, each identified by an SL-7 number and an AD- number. A list of all SL-7 reports available to date is included in the back of this report.

This report documents the installation of the long-term stress recorders and the method involved in selecting and converting the raw stress data to histograms. The reduction of a seven-year collection of these data are presented.

Rear Admiral, U.S. Coast Guard Chairman, Ship Structure Committee

## Technical Report Documentation Page

1. Report N	lo.	2. Go	vernment Access	ion No.	3. R	ecipient's Catalog N	•.
SSC-3	304 (SL-	7-26)	)-A11-	1055			
4. Title on	d Subtitle	F11/			5 R	eport Date	
		ess Data Coll	ection and			June 1, 198	1 1
	ction		200.01. 41.4		A P	erforming Organization	
ive.du	C C 1 O II				0. F	errorming Organizati	on Code
7. Author/s	)		-		8. Pa	erforming Organization	on Report No.
	. Booth					SR-1245	
	ng Organization Non yne Engineer				10. V	Work Unit No. (TRAI	5)
	ear Hill Road				111	Contract or Grant No	
	am. MA 02154					CG-844331-A	•
**********	om: 11/1 Oz.20	•				<del></del>	
13 6		* * * * * * * * * * * * * * * * * * * *			7	Type of Report and P	eriod Covered
	ing Agency Name an	id Address			F	inal Report	1
	Coast Guard				] 1	972-1981	į
Uffic	e of Merchan	it Marine Saf	ety		<u> </u>		
Washi	ngton, D.C.	20593	. ,		14. s	iponsorina Agency C G-M	od•
15. Supplem	nentary Notes						
Perfo	rmed under U	ISCG contract	for the	interagency S	hip S	Structure Com	mittee
							į
16. Abstrac	<del></del>					······	<del></del> ,
				ar period is			
17. Key Wo	.d.		<del></del>	18. Distribution Stat			
·			ļ			able to the	II C Dublia
Extre	me Stress Sc	ratch Gauge	l				
		J	l				1 Information
				Service, Spr	ingfi	eld, Virgini	a 22161
							i
19. Securit							
	y Classif. (of this re	pport) 20	. Security Class	if, (of this page)		21. No. of Pages	22. Price
Unc1	y Classif. (of this re	pert) 20	. Security Class Unclass	· •		21. No. of Pages 72	22. Price

Form DOT F 1700.7 (8-72)

Reproduction of completed page authorized

METRIC CONVERSION FACTORS

	Symbol		.5	•	e !	P. ē			~ <u>e</u>	Ĵ₽.	,				<b>3</b> 4	2				8	K i	÷ .	i?		!						2 2 2	T 5 .
c Measures	To find		į	segger	feet	2 P. P. S			source mechas	Square yards	square miles	5			- 50,000	Spends chart tons			•	fluid aunces	pints	Sheup	10017	Spire Digital			=	1	Fahrenhait		2 002 091	00
rsions from Metri	Muttigly by	LENGTH		Š •	3.3	0	}	AREA	91.0	2		ç;		MASS (weight)	0.036	77	<u>:</u>	VOLUME		0.03	2.1	1.06	0.26	χ.	?		TEMPERATURE (exact)		9/5 (then	() Pr mon	386	2000
Approximate Conversions from Metric Measures	When You Know			Contimeters	meters	meters				Square meters	Square kilometers	hectares (10,000 m <sup>-</sup> )			grams	hilograms	(84 0001) semos		•	millitions	liters	liters	liters	cubic meters	Cobic meters		TERM		Cetsius	temperature	33	-20
	Symbol			ŧ	E	<b>6</b> -	5		٦	Ē~E	<b>~</b> §	2			•	2	-			ē	· <b>-</b>	-	_	~E′	È				٥			
ez	zz Lunia	ız	oz			**			<b>91</b>	SI		••	E		<b>z:</b>   			o1	1	i Ma			1		,			` ` !		111	· (2	cm
	rri	111	Մ	' l'	'1	     <sub>7</sub>	'['I		'''  	'l'  •	<b>'</b> 1'	'''  	- 1	' '   s	'l' '	ľľ	"	' '	   	'l'	'l'	3	<b>'</b>  '	!'  	' <b>1</b> '	'I'	'   -  -	' ' 	'	l'[ˈ	T   11   1	inches
		Symbol				£ 5	ŧ.	5				` <u>`</u>	2			<b>.</b> .	E*				Ē 1	Ē	: -		-	_'	<b>"</b> E '	Ē			υ	H. 286.
Measures		To find Symbol				contimeters cm		kilometers km		Secretary Continues Cres		square motors m <sup>2</sup>					Kilogrāma kg tomnes t					militare m		liters	liters	litters !		cubic meters m <sup>3</sup>			Celsius temperature	salies, our MIS Abos, Pobl. 276,
versions to Metric Measures			3 H & 3 H &				meters	kilometers	AREA		squara meters	square moters					Kilograms tonnes		VOLUME		millitters.					friers	cubic meters	cubic meters	ERATURE (exact)		a volca	requires, test mare thrustest substem, that MilS Mrs., Publ. 276, (D. Lesting, No. C.) 10 Tab.
Approximate Conversions to Metric Measures		To Find	1 F C 2 M -			Contineters	0.9 meters	1,6 kilometers	AREA	a political post of the second	square meters	0.8 square motors	hectores			28 grams	Kilograms tonnes	-	ACCUME		S. Millitars	45 militare			\$6.0	3,8 inters	et 0.03 cubic meters	s 0.76 cubic meters	TEMPERATURE (exact)		Celsius temperature	of the C. 2 file councility, the more extra convergency performer detailers tables, one MIS New, Pool 276, Units of Recipion and Mesoners, then 9.25, SD Leaving No. C.53 to 786.

METRIC CONVERSION FACTORS

### CONTENTS

		Page
I.	BACKGROUND	1
II.	FUNCTIONAL DESCRIPTION	1
III.	VESSEL DEPLOYMENT AND EQUIPMENT HISTORY	6
IV.	DATA PRESENTATION AND INTERPRETATION	3
٧.	DISCUSSION	36
VI.	SUMMARY	37
VII.	ACKNOWLEDGEMENT	37
	APPENDIX A - SCRATCH GAUGE INSTALLATION	38
	APPENDIX B - RECORDER CALIBRATION DATA	41
	APPENDIX C - HISTOGRAM COMPUTER LISTING	45
	APPENDIX D - DATA AVERAGES	47

Acces	nion For	e.yee
NTIS	GRARI	XI.
DTIC	TAB	7
Unann	<b>becau</b>	
Justi	fiestion	
	<del></del>	
Bv		
Distr	ibution/	
Avai	lability C	odes
	Avail and	/or
Dist	Special	
	1	
1 /1 -	]	
17		
-		



٧

#### BACKGROUND

This seven-year data collection program has been conducted in three phases. The first three years of the program were conducted under Department of the Navy Contract NO0024-73-C-514D. Serial No. SF35422306 Task 2022, SR215. The next two years were conducted under Coast Guard Contract DOT-CG-61712A. Report SSC-286(SL-7-25) covering the first five years was published by the Ship Structure Committee in 1979. The final two years of data collection was also sponsored by the Ship Structure Committee, Contract No. DOT-CG-844331-A. Project SR-1245-SL-7 "Extreme Stress Data Collection and Reduction." The present report collates data from the final two years with data previously reported, to provide a comprehensive summary of all the data.

Nine N.C.R.E. mechanical strain-gauge recorders were installed on the eight SL-7 high-speed containerships operated by Sea-Land Service. Inc. These vessels operated on both transatlantic and transpacific routes.

#### 11. FUNCTIONAL DESCRIPTION

The purpose of this program was to obtain as much midship bending stress data from the SL-7's in the simplest and most direct manner possible. To meet this requirement, N.C.R.E. (Naval Construction Research Establishment) maximum-reading strain-gauge recorders and clock units (Figures 1 and 2) were obtained from Elcomatic Limited of Glasgow. Scotland. The units were installed at approximately midships in the starboard longitudinal box girder (tunnel) of all eight SL-7s (see Appendix A for installation details).

The N.C.R.E. strain gauge consists of contact points 10 inches apart and a mechanical linkage which provides a magnification of approximately 100:1 at the stylus. The stylus moves against a pressure-sensitive recording paper causing both positive and negative deflections to be indicated by a scratch mark (Figure 3). The paper is indexed about 0.1 inch every four hours. Once every sixth interval (i.e., every 24 hours) the index is 0.4 inches wide. Each vertical marking has a length which represents the maximum peak to maximum trough stress which has occurred during the four-hour period during which the stylus was at one place on the paper. For accurate data interpretation, it is important to remember the following characteristics of this system:

- 1. The record indicates the combined wave-induced and first-(or higher) mode vibratory stresses; there is no way to separate the various effects.
- 2. The maximum peak, and maximum trough stresses indicated on the record may not have occurred as part of the same cycle; i.e., they may have occurred at different times during the four hour record interval (Figure 4).
- 3. Slow "static" changes in the average stress caused by thermal effects. ballast changes, etc., will contribute to the total length of the scratch line. Appendix D of this report provides further information on these slow changes.

1

# N.C.R.E.-maximum reading STRAIN GAUGE RECORDER

The analysis of wave-induced stresses imposed on the steel hull of a surface vessel involves the use of data relating to maximum bending moments applied to the hull girder. In the course of such analysis, scientific staff of the Naval Construction Research Establishment, Dunfermline, Scotland, adopted a method of recording maximum strain variations during specified time intervals by means of a maximum-reading strain gauge incorporating a strip chart.

Prototype quantities of the NCRE designed recorder were produced within the Establishment, subsequently evaluated and used as highly successful data acquisition instruments in the arduous environments experienced by Royal Navy warships at sea. To meet a demand for further models, it was decided by NCRE to permit a strain instrumentation company to manufacture the device commercially. Elcomatic Limited of Glasgow was chosen, and the NCRE recorder now is available as a standard Elcomatic product.

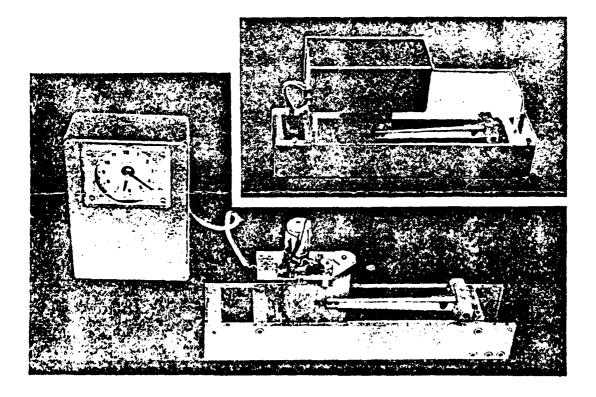
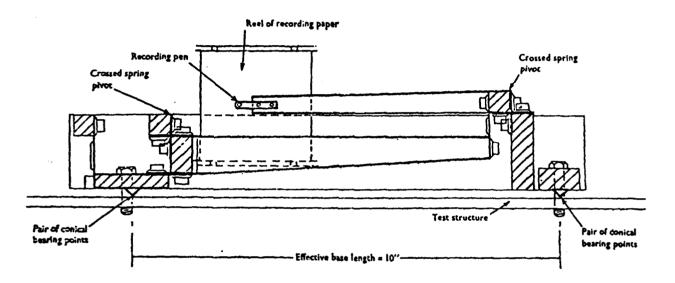


FIGURE 1

#### Gauge Action:

As shown in the sectional diagram below, the lever system is actuated by distortion of the structure under test and requires no external power supply. The instrument is bolted in position, bearing against the test surface on two sets of hardened conical studs. Any change in separation of bearing points is magnified by the lever system which drives the recording pen across the stationary reel of carbon-backed paper. Time related maximum strain records are obtained by forward movement of recording paper programmed by a precision battery-rewound clock and powered by a small motor also battery powered.



Details:		Linearity	Substantially linear over strain range of 0,0025.
Prime function	Fully automatic recording of maximum strain.	Temperature effects	Uniform temperature changes of gauge and
Duration of Continuous unattended operation Magnification Factor	Three months depending on programme. Nominally 100—subject		steel test structure pro- duce no discernible pen movement.
	to precise calibration by a dial gauge reading to 0.0001".	Vibration	Tested by dynamic strains of double amplitude 0.0008 at frequencies 25
Resolution	A strain change of 0.001 will produce a 1" pen deflection.	Chart loading	to 200 cycles per minute— no significant inaccuracy. Cassette.

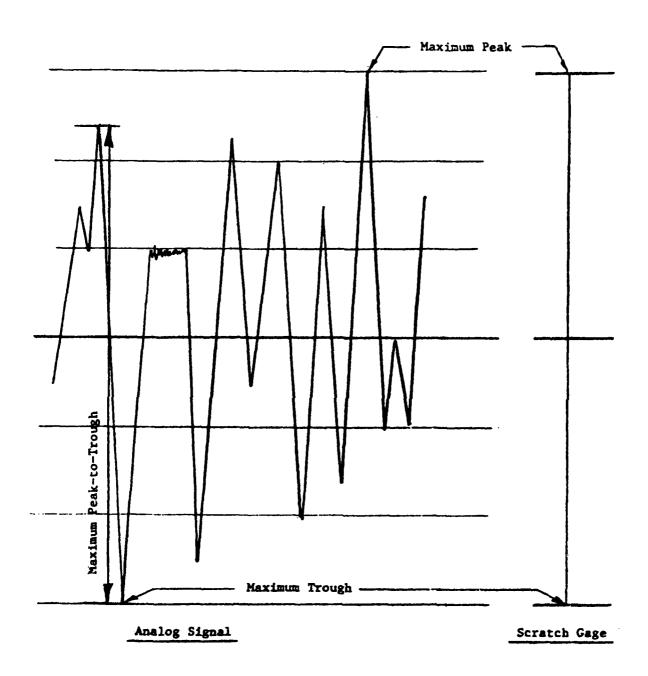
FIGURE 2

			,
_	<del></del>		
	į		
	į		_ `
	1	-	0
			e :
_	<del>ا جو ب</del>		¥
	2,2		Beckman'
	-		<b>.</b> ≛. ¦
			:
	,		•
_	ے_		<i>:</i>
	ے ج		:
	بيآ		
			i
,			1
L			
	ت د		i
			:
	_	<b>建加多等。 《重要要》</b>	
ř			
			,
			نـــــ
	=		
	ce?		
	7		
ř			- :
-			
			•
	_م_		ا نـــــ
سم،لسته بن	<u>ب</u> مـــ		' اـــــــ ا
مه النسم ، أسماله ما	ر. دوري		 أ
	-0.		   
La Read Land Hard Land	9.		   
A DELLE LAND BURNER BURNER BERTER	_ <del></del>		 !
A bear lead to the same and the same and the	- a,		
14 14 14 14 14 14 14 14 14 14 14 14 14 1	-0.5		
ومستعفة المالحكيكية بندوسة للندور أسروو بد			
1000 0-000 000 000 000 000 000 000 000 0			
منتدة ملق و بلامة ، إن لهذي كللة ربيعة في الدرو ، أ يروع و و			
24 10 10 10 10 10 10 10 10 10 10 10 10 10			
المستقلة مستقدة منف وسيديد إلى لهم عكلان بيدي والدرور أيدروو با			
فانسا فسنكف سنتينه منف وسيدين إيران ملكندة بيده في والمربر أير عد يد	disconnection of the		
فتنافقان عد أعينكا فدجوت ومراد ومرادي إلى ليطرع كنان بلاواره والمرور أيدروا	die		
التانا الانامنية عد أعينك المستكنة ملك مدرية على أما لها كاللاز بنية في المدرية المدرية	difference of the second		
المناقلة المنافئة المسلمين المستقلية والمراجية والمنافية أما الملاعكة والمدار المستوالين والمستوالي	Contract Charles		
فقة مانناكاتاناتة نامنها بمسأعين منافيه وتناب وسيديد إلى لهذي كللة وللهادة الدورة الدروع والمدورة	State State		
والمستعلقة والمنافقة والمنتازين والمستعدد والمراور والمرا	dien dien		
المستنافة المقافة المنافقة المنافئة والمستفيدة والمناور والمناول المنافة المنافقة والمنافقة المنافقة المنافقة والمنافقة والمنا	district district		
المستقلة المستقلة والمستورة والمستوري والمستور والمستور والمستوري والمستوري والمستوري والمستوري والمستوري	State Contract		
1	State Contract		
المراجعة المستوان المراجعة المستوان المستوان والمراجعة و	State Contract		
1	State Contract		
	State Contract		

g ···	grapria <u>presidentali i di ila ki mera di</u>
1	<u></u>
3	F
1	<u></u>
3	
궑	
ě.	
3	
9	Esta Batalga a popular
1	
3	
g	
ěj.	
Ş	
3	
ā	
ង	
d	00/2
ă	
p .	
9	
þ	
8	
Ē	######################################
= ~	
3	
ě.	<b>ニイ</b> ンクニーニー
= -	
KA KA	
3 4	i (7 = = = = = = = = = = = = = = = = = =
£ 3	
Ŋ,	
2	
ā	
CARACTE CONTRACTOR OF THE CONTRACT OF THE CONT	
3	<u> </u>
3	
i	
	RESIDENCE TO A PROPERTY OF THE PARTY OF THE

SEALAND MCLEAN VOYACE #5 PORT SIDE

SAMPLE DATA TAPE FIGURE 3



ILLUSTRATED EXAMPLE OF THE COMPARISON OF AN ANOLOG SIGNAL WITH THE SCRATCH GAGE

FIGURE 4

Prior to installations, each scratch gauge was calibrated utilizing a Bridgeport milling machine. The fixed collet and moveable table were used to generate strain. The table was moved in both tension and compression directions in increments of 0.001 inches, with a dial indicator used to measure the amount of displacement. A calibration table and plot for each instrument is provided in Appendix B of this report.

All of the scratch-gauge recorders and clock units have been removed from the vessels and returned to TES for storage. Each recorder was checked to insure that its calibration was still valid. No significant change in calibration was found.

#### III. VESSEL DEPLOYMENT AND EQUIPMENT HISTORY

The following section is a brief summary of each vessel's routing assignment from the time the scratch gauge(s) were installed until their removal. Included are comments concerning the operation of the equipment. The sequence is in the order in which the equipment was installed and placed in service.

The eight SL-7s have been utilized on either a transatlantic or transpacific route. Atlantic crossings involve some or all of the following ports: Port Elizabeth, N.J.; Portsmouth. VA; Bremerhaven. Germany; Rotterdam, Netherlands; and Algeciras. Spain. Those vessels assigned to Pacific duty followed a steady route that began in Seattle, Washington. with calls in turn at Long Beach, California; Oakland, California; Yokohama, Japan; Kobe, Japan; and Hong Kong.

For the first few years, the vessels operated at their designed speed of 33 knots. After the price of fuel quadrupled in the mid-seventies, the vessels' speed was reduced to 20-24 knots to conserve fuel and reduce operating costs.

#### 1. SEA-LAND MCLEAN

This vessel became the test bed of the eight SL-7s. The hull and numerous components were heavily instrumented to investigate bending and torsional hull response. The data were published by the Ship Structure Committee as part of its SL-7 library. Two scratch gauges were installed October 7, 1972 (Serial No. BS72E0001 in the port tunnel, and Serial No. 026 in the starboard tunnel). Teledyne engineers rode this vessel for the winter months of 1972 to 1975 and were able to monitor the scratch gauges daily during this period. The McLean sailed the Atlantic until May 1975. When she transferred to the Pacific after a dry-docking at Newport News, Virginia.

In order to ascertain if the calibration curve for an installed unit had changed with time, the McLean port tunnel gauge was removed on October 18, 1975 and replaced with the spare unit (Serial No. BS73E0001). The removed unit was returned to TES and recalibrated. See Appendix B for the results of this test.

Both instruments performed well up to the time of their removal on September 14, 1980. One clock unit failed in May 1978, and one roll of tape from the port gauge was lost due to loss of stylus pressure in April-May 1979.

#### 2. SEA-LAND GALLOWAY

Gauge unit Serial No. BS73A007 was installed in the starboard tunnel on March 10, 1973. A problem with excessive moisture condensation in the tunnels during the winter months was solved by placing a plexiglass enclosure around each unit and using a 40-watt light bulb as a heat source. Both the Galloway and McLean were retrofitted with this arrangement, and it was included for all subsequent installations. The Galloway started in Atlantic service, transferred to the Pacific in September 1973, and then returned to the Atlantic in December 1975.

Data output from the <u>Galloway</u> has not been up to a par with the other vessels. Numerous nagging problems encountered over the years include clock failures, broken wires, improper stylus pressure. loose screws, and a constant crew change.

#### 3. SEA-LAND COMMERCE

Scratch-gauge Serial No. BS73A002 was installed on May 2, 1973 prior to the ship sailing for Pacific duty. The Commerce has remained in the Pacific ever since. The data from this ship have been good. Early problems included a defective drive motor and clock failure. Periodic clock and switch problems occurred, but did not cause any major interruptions of data collection. The unit was removed from service September 10, 1980.

#### 4. SEA-LAND EXCHANGE

Scratch-gauge Serial No. BS73A004 was installed on May 13. 1973. The vessel stayed in Atlantic service until November 1973, when she transferred to, and remained in, the Pacific. With the exception of clock problems in 1975, the data received from this vessel have been excellent. The credit for this must go to the Chief Engineer, who took a personal interest in this project and provided on-board care for the unit.

Removal was on April 12, 1980 during a regular service call. The entire recorder drive chain of gears had stripped. It was also anticipated at that time that the SL-7s would be out of service by mid-summer because of their expected sale to the U. S. Government.

#### 5. SEA-LAND TRADE

Scratch-Gauge Serial No. BS73A008 was installed on May 22, 1973. The vessel transferred immediately to Pacific Service and remained there. This system performed well until May, 1976, when the dynamic response data did not seem to match data from other Pacific vessels. In September, 1977 the unit was removed and Serial No. BS72E001 (the original McLean port gauge) was installed. The quality of the data returned to normal. The problem was found to be caused by the misalignment of the mechanical multiplier arm. With this exception this unit produced excellent data, and credit must go to the two Chief Engineers who provided the on-board care. The unit was removed from service on September 25, 1980.

#### 6. SEA-LAND FINANCE

Scratch-Gauge Serial No. BS73A005 was installed October 3. 1973 prior to her departure for the Pacific, where she remained. A broken mounting stud was repaired in June 1974 and a clock replaced in October 1979. The unit was removed September 28, 1980. This unit has produced good data during its entire service.

#### 7. SEA-LAND MARKET

Scratch-Gauge Serial No. BS73A003 was installed on November 5, 1973. This vessel has remained in Atlantic service during her operational life. Clock problems were encountered during the first year, and switch problems during 1979. With these two exceptions, the unit has been satisfactory. The unit was removed from service on November 13, 1980.

#### 8. SEA-LAND RESOURCE

Scratch-Gauge Serial No. BS73A006 was installed on December 13. 1973. This ship was originally assigned to the Pacific, but returned to Atlantic service late in 1974. This unit was plagued with problems during its entire service. Stylus problems occurred in 1974-1975 and again in 1979. Clock failures occurred in 1976-1977-1979 and early 1980. In addition, a number of data tapes were lost in the mail. The unit was removed October 30, 1980.

#### SUMMARY

Most of the systems have performed well. The battery-operated clock is the major weak link. Periodic routine maintenance is required to keep these systems at top performance. On-board care was reduced to changing tapes and batteries. Usually, the Chief Engineer of each vessel undertook this responsibility. He also annotated the tapes with the date and time periodically. In general, the cooperation was excellent throughout the entire program.

#### IV. DATA PRESENTATION AND INTERPRETATION

As previously stated, the data have been collected on rolls of pressure-sensitive paper. Each roll represents approximately three months' time and usually, at least, 2 rolls of tape are collected during each six-month visit to the vessel. In order to protect the data and facilitate analysis, each data roll was subsequently mounted on  $8\ 1/2\ x\ 11$ " card stock with usually 3 strips of the roll mounted per sheet. This is approximately two weeks of real-time data.

The length of each data marking (scratch) has been measured to the nearest 0.02 inch and the results tabulated for each vessel over the seven data years of information collected. It is this data tabulation which supplies the basis for the histograms which are presented in the following pages. In order to present the data in a more useful form (i.e., psi of midships bending stress vs. number of occurrences) it was necessary to perform the following transformation:

Since the scratch gauge is substantially linear, its calibration curve is approximated by a straight line, and this by the equation

$$y = Mx + B$$

where

y = stylus deflection in inches

 $\ddot{X}$  = hull girder elongation in 10 inches

B = slope intercept

M = slope of the calibration curve around the point of interest

If we assume that the scratch gauge operates around the zero points; i.e., there is no constant stress and any offset due to loading is ignored, "B", the slope intercept, is zero.

Solving for X:

$$X = \frac{y}{M}$$

Stress (psi) = (E. Young's Modulus for Steel) (Elongation in 1 inch)

$$\sigma = (30 \times 10^6) (\frac{y}{M} \times 10^{-1})$$

and

$$\sigma = (3 \times 10^6) \frac{y}{M}$$

or

$$\sigma$$
 psi =  $\frac{(3 \times 10^6)}{(\text{slope of the best straight line approximation})}$ 

The lengths of the scratch lines have been tabulated. The slope of the calibration curve for each vessel has been derived from the calibration plots of Appendix B and is tabulated in Table I. Since the majority of the data points lie between a gauge deflection of +0.4 inches to -0.4 inches, the slope of the line was calculated between these two values. The stress value for each data interval, therefore, can be calculated from:

The scale factors have been calculated for each gauge and are presented in Table II. Thus, all the information to prepare histograms of stress levels versus the number of occurrences has been developed.

Calibration         Slope         Curve         Value         SCRATCH GAUGE         SCALE FACTOR           M:LEAN PORT         B-1         87         MCLEAN PORT         S.CRATCH GAUGE         SCALE FACTOR           M:LEAN PORT         B-1         87         MCLEAN PORT         3.448 x 10 <sup>4</sup> Poriginal         B-2         88         Original         3.125 x 10 <sup>4</sup> Spare (Replacement)         B-3         96         Spare (Replacement)         3.125 x 10 <sup>4</sup> GALLOWAY         B-6         91         GALCOWAY         3.297 x 10 <sup>4</sup> COMMERCE         B-6         91         GALCOWAY         3.297 x 10 <sup>4</sup> EXCHANGE         B-7         91         EXCHANGE         3.409 x 10 <sup>4</sup> FINANCE         B-9         FINANCE         3.409 x 10 <sup>4</sup> RESOURCE         B-10         82         MARKET         3.699 x 10 <sup>4</sup> RESOURCE         B-11         86         RESOURCE         3.499 x 10 <sup>4</sup>	SLOPES OF CALIBRATION CURVES	RATION CURVES		DATA MULTIPLICATION SCALE FACTORS	CALE FACTORS
al         B-1         87         MCLEAN PORT           bration         B-2         88         Original           creplacement)         B-3         96         Spare (Replacement)           B-4         94         MCLEAN STBD           B-5         91         GALLOWAY           B-6         88         COMMERCE           B-7         91         EXCHANGE           inal)         B-8         97         TRADE (Original)           acement)         B-2         88         (Replacement)           B-9         99         FINANCE           B-10         82         MARKET           B-11         86         RESOURCE	Scratch Gauge	Calibration Curve (Fig.)	Slope Value	SCRATCH GAUGE	SCALE FACTOR
iginal         B-1         87         MCLEAN PORT           calibration         B-2         88         Original           are (Replacement)         B-3         96         Spare (Replacement)           STBD         B-4         94         MCLEAN STBD           NY         B-5         91         GALLOWAY           N         B-6         88         COMMERCE           iE         B-7         91         EXCHANGE           ic         B-8         97         TRADE (Original)           ic         B-9         99         FINANCE           B-10         82         MARKET           B-11         86         RESOURCE	EAN PORT				
calibration         B-2         88         Original           calibration         B-3         96         Spare (Replacement)           STBD         B-4         94         MCLEAN STBD           STBD         B-5         91         GALLOWAY           K         B-6         88         COMMERCE           BE         B-7         91         EXCHANGE           Keplacement)         B-8         97         TRADE (Original)           Replacement)         B-9         99         FINANCE           B-10         82         MARKET           B-10         86         RESOURCE	Original	8-1	87	McLEAN PORT	V
Acted (Replacement)         B-3         96         Spare (Replacement)           STBD         B-4         94         MCLEAN STBD           N         B-5         91         GALLOWAY           E         B-6         88         COMMERCE           StE         B-7         91         EXCHANGE           Original)         B-8         97         TRADE (Original)           Replacement)         B-2         88         FINANCE           B-10         82         MARKET           B-10         82         MARKET           B-11         86         RESOURCE	Recalibration	B-2	88	Original	$3.448 \times 10^{7}$
STBD       MCLEAN STBD         AY       B-5       91       MCLEAN STBD         AY       B-6       88       COMMERCE         SE       B-7       91       EXCHANGE         GOriginal)       B-8       97       TRADE (Original)         Replacement)       B-2       88       (Replacement)         B-9       99       FINANCE         B-10       82       MARKET         B-11       86       RESOURCE	Spare (Replacement)	B-3	96	Spare (Replacement)	$3.125 \times 10^{7}$
AY         B-5         91         GALLOWAY           E         B-6         88         COMMERCE           iE         B-7         91         EXCHANGE           Original)         B-8         97         TRADE (Original)           Replacement)         B-2         88         (Replacement)           E         B-9         99         FINANCE           B-10         82         MARKET           E         B-11         86         RESOURCE	MCLEAN STBD	8-4	94	McLEAN STBD	$3.191 \times 10^{4}$
E	GALLOWAY	8-5	91	GALLOWAY	$3.297 \times 10^{4}$
iE         B-7         91         EXCHANGE           (Original)         B-8         97         TRADE (Original)           (Replacement)         B-2         88         (Replacement)           E         B-9         99         FINANCE           B-10         82         MARKET           E         B-11         86         RESOURCE	COMMERCE	8-6	. 88	COMMERCE	$3.409 \times 10^{4}$
Original) B-8 97 TRADE (Original) (Replacement) B-2 88 (Replacement) (Replacement) E B-9 99 FINANCE B-10 82 MARKET (E B-11 86 RESOURCE	CHANGE	8-7	91	EXCHANGE	$3.297 \times 10^{4}$
(Replacement)       B-2       88       (Replacement)       3.409 x         E       B-9       99       FINANCE       3.030 x         B-10       82       MARKET       3.659 x         E       B-11       86       RESOURCE       3.488 x	ADE (Original)	8-8	26	TRADE (Original)	$3.093 \times 10^{4}$
E B-10 82 MARKET 3.659 x 3.488 x RESOURCE 3.488 x	(Replacement)	8-2	88	(Replacement)	$3.409 \times 10^{2}$
B-10 82 MARKET 3.659 x 3.488 x RESOURCE 3.488 x	AANCE	8-9	66	FINANCE	$3.030 \times 10^{7}$
3.488 x 3.488 x	KET	8-10	82	MARKET	$3.659 \times 10^{7}$
	SOURCE	8-11	86	RESOURCE	3.488 x 10 <sup>+</sup>

The histograms are arranged in the order of data years. One histogram is provided for each gauge for each year. (In data year five, 2 histograms are provided for the SEA-LAND TRADE as two gauges of different calibration factors were used).

Associated with each year are three additional plots. A summary plot of all Atlantic data, a summary plot of all Pacific data, and a final plot of all data collected within the year. Finally, three summary total histograms are included: A seven-year Atlantic summary, a seven-year Pacific summary. and a summary of all data collected during the seven-year period. Thus, a total of 88 histograms are presented (Figures 5 through 92, inclusive).

To facilitate data presentation, the data have been divided into "Data Years" as follows:

Data Year (1)

September 1972 to May 1, 1974

The first year has been broadened to include the early contractual period which started in September of 1972 rather than starting with May 1, 1973, primarily because only the MCLEAN and GALLOWAY had their installations in operation prior to the May 1, 1973 date. Data year seven has also been expanded to include the remaining months of 1980 prior to system removal.

Data Year (2)

May 1, 1974 - May 1, 1975

Data Year (3)

May 1, 1975 - May 1, 1976

Data Year (4)

May 1, 1976 - May 1, 1977

Data Year (5)

May 1, 1977 - May 1, 1978

Data Year (6)

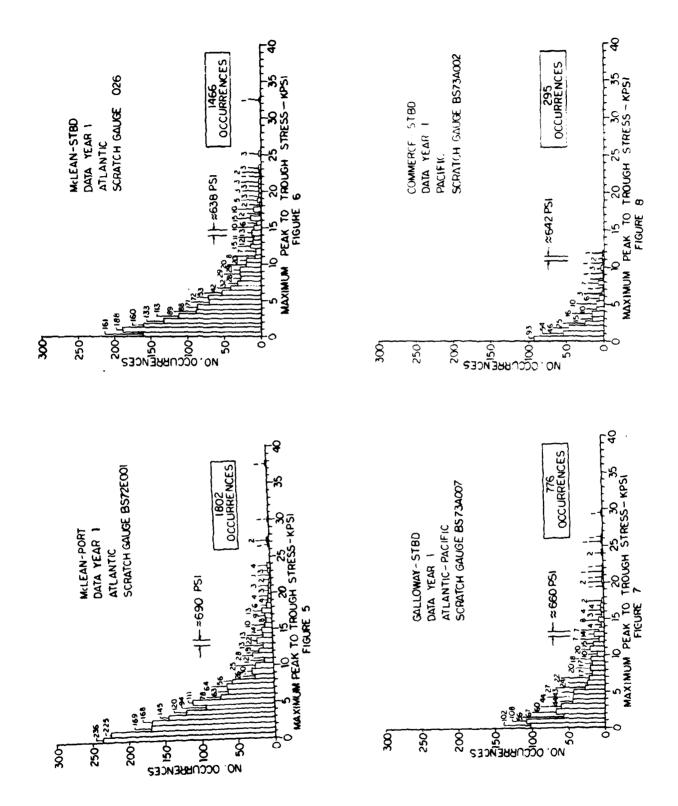
May 1, 1978 - May 1, 1979

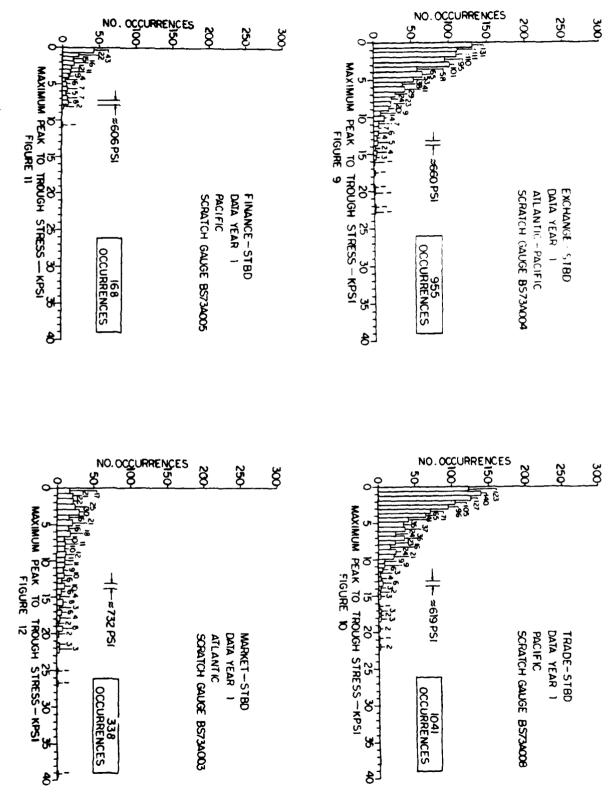
Data Year (7)

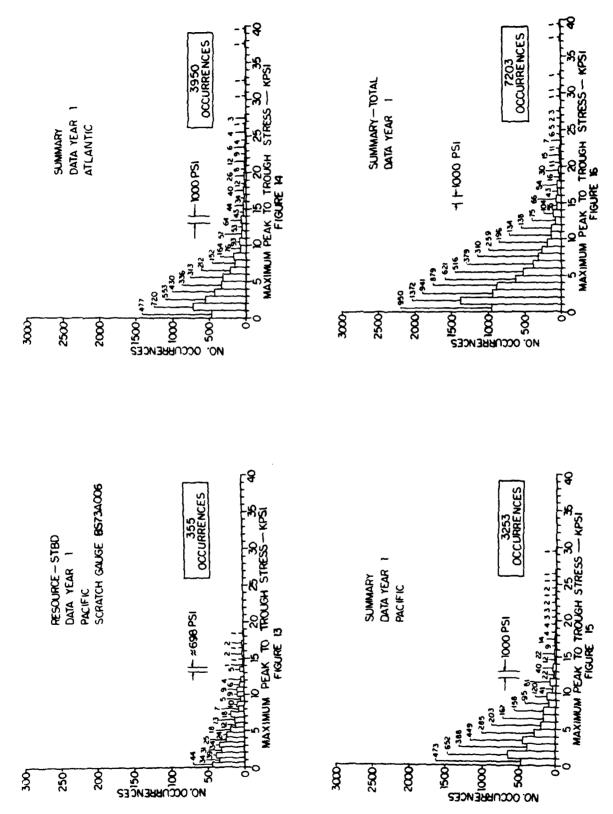
May 1, 1979 - Fall 1980

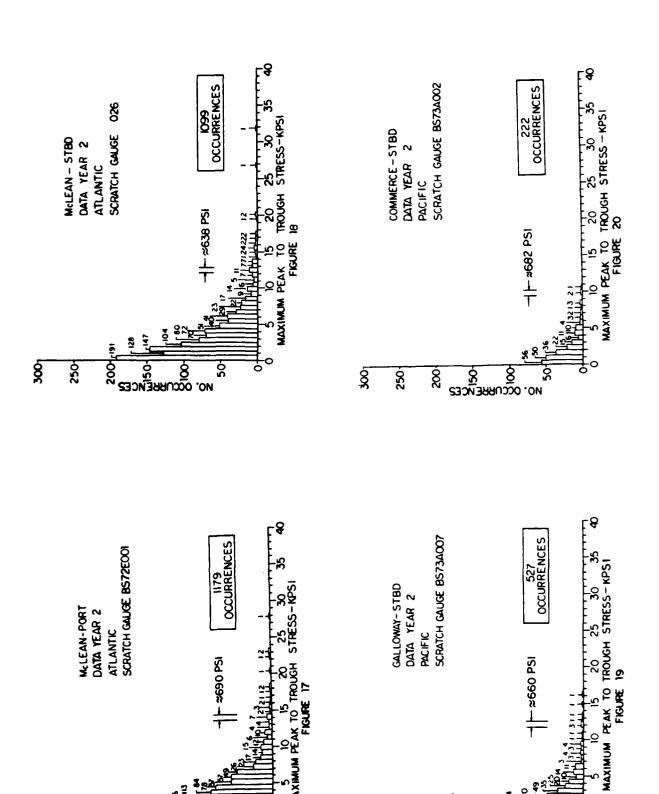
As part of this contract, it was desired to establish a correlation between the McLean scratch-gauge data and tape-recorded stress data from the longitudinal vertical bending stress transducers in operation during the first two winter seasons.

(Text continues on Page 34)









ğ

250

NO. OCCURRENCES

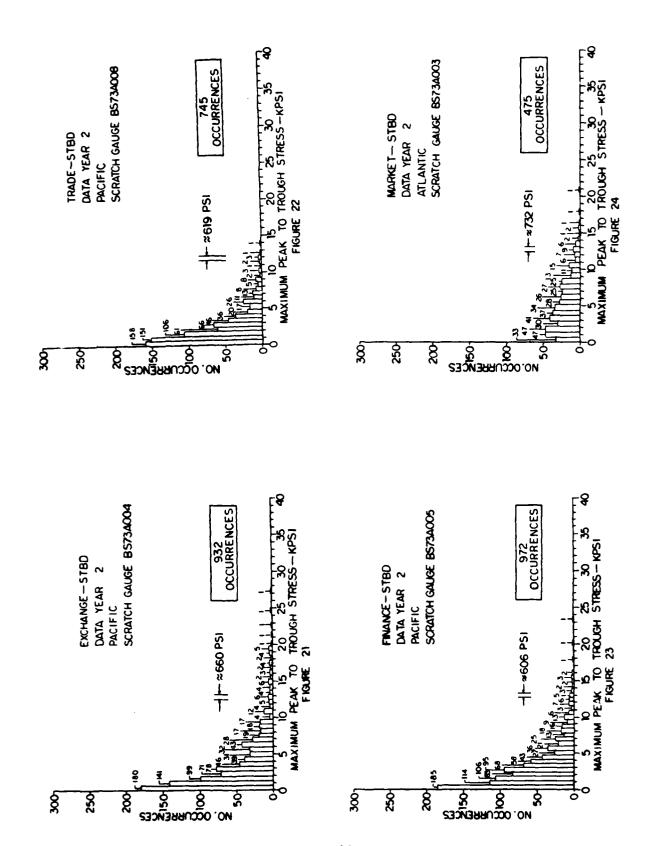
ğ

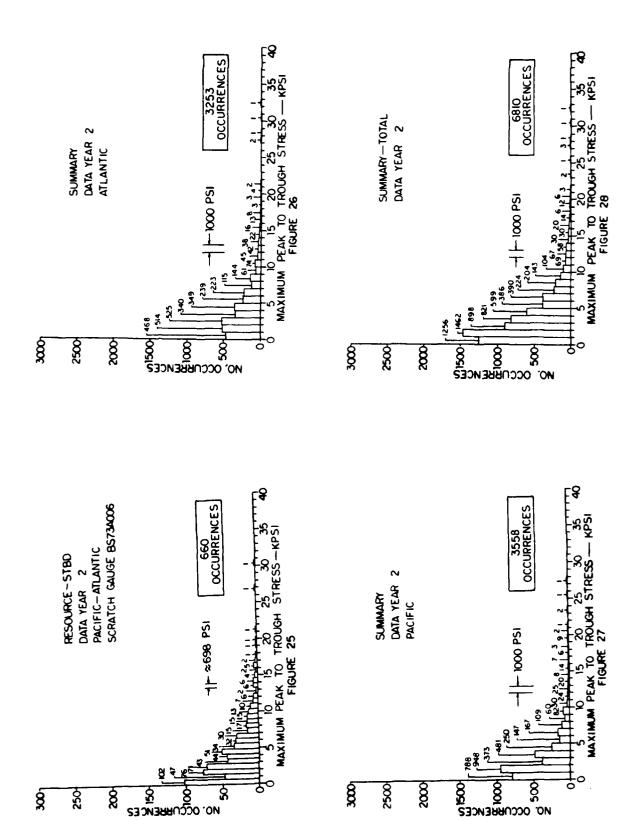
**2**50

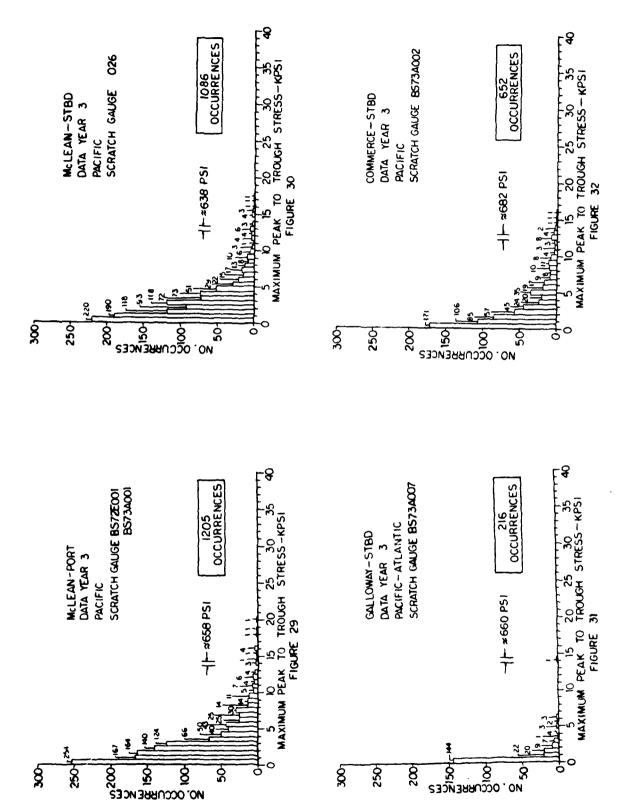
8

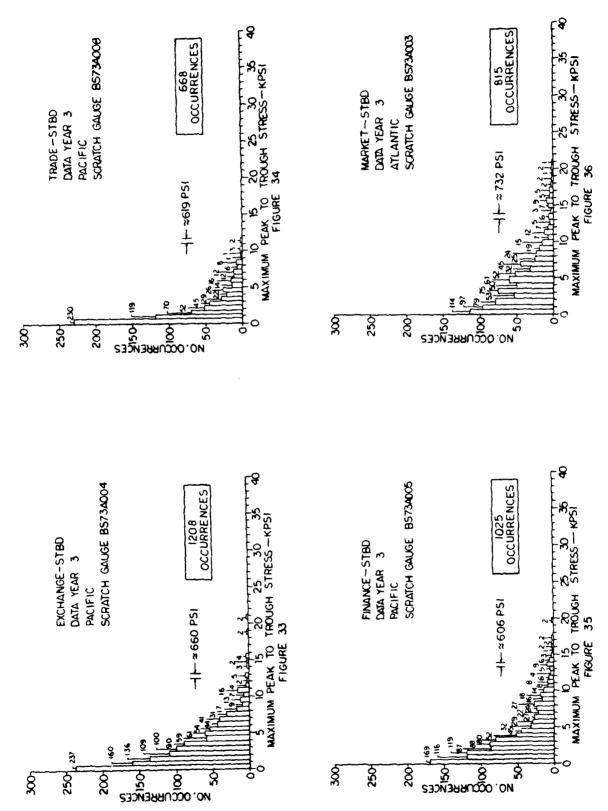
OCCURRENCES

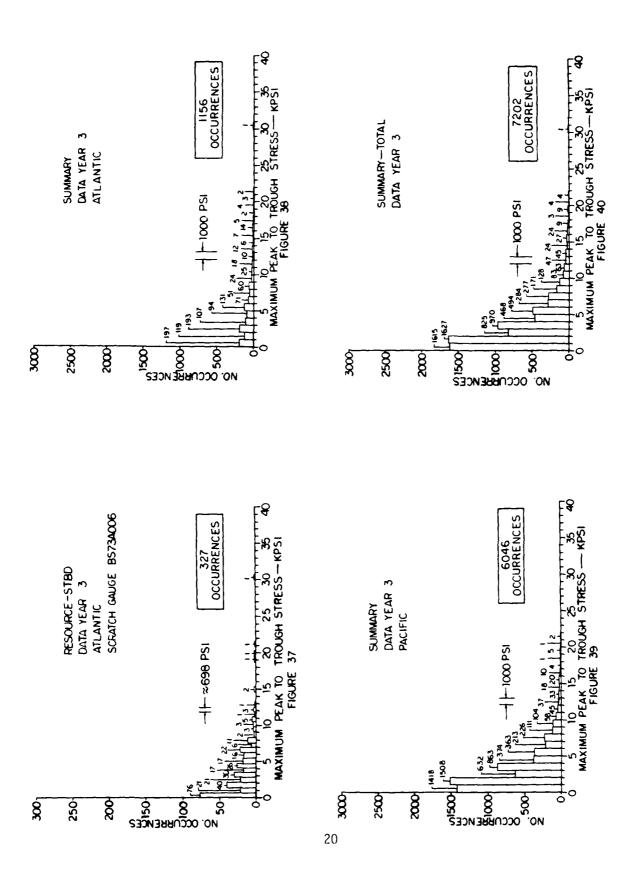
.wo. 504)

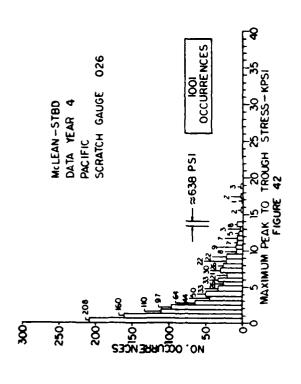


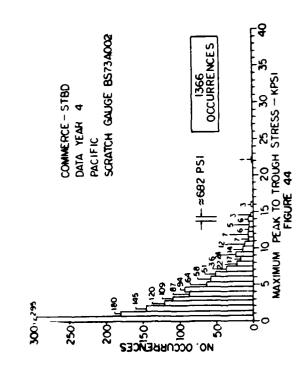


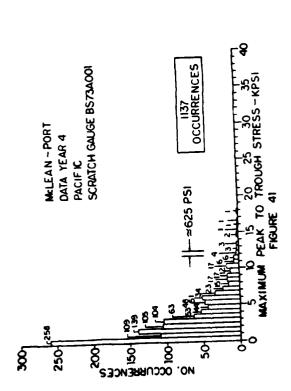


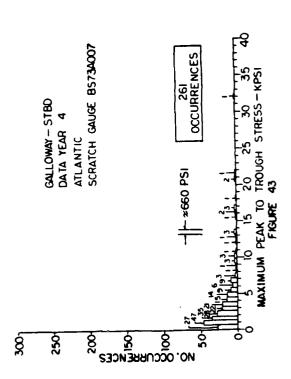




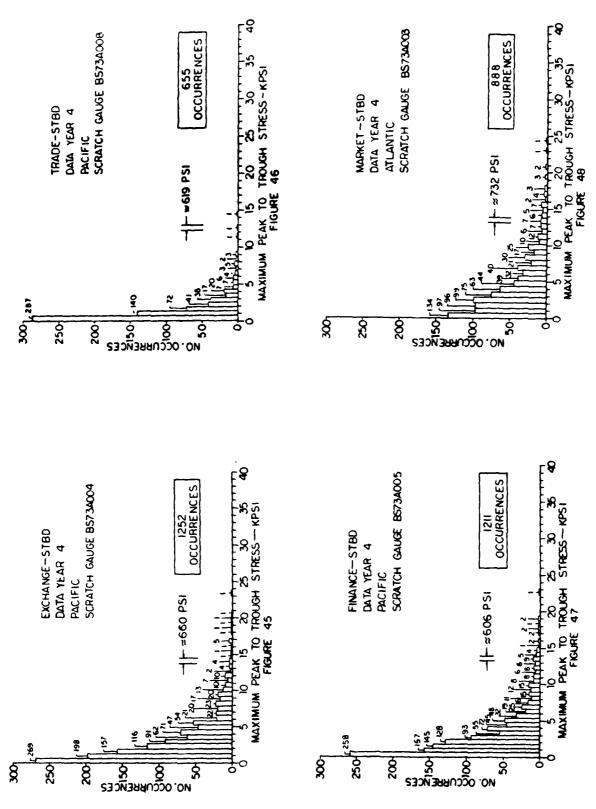


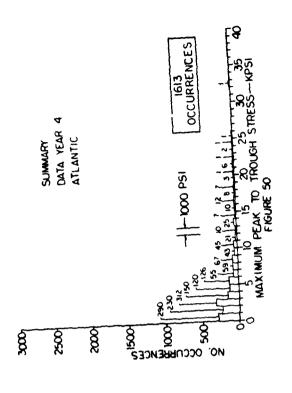


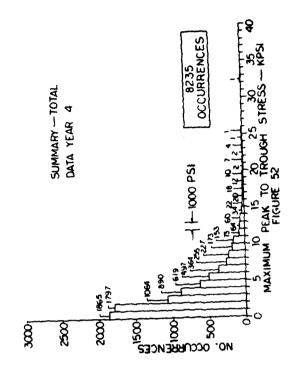


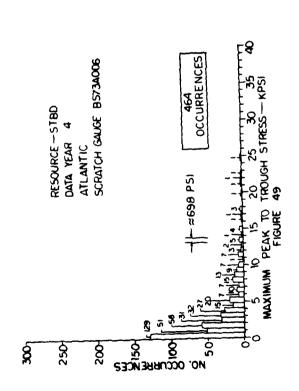


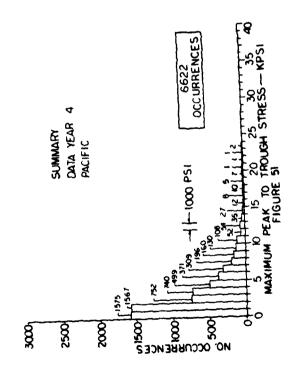
• • • •



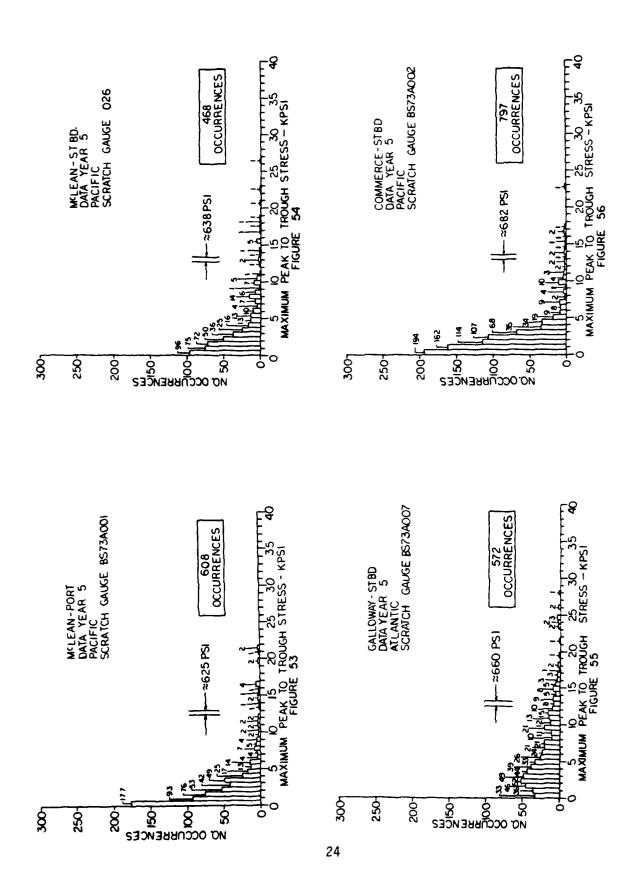


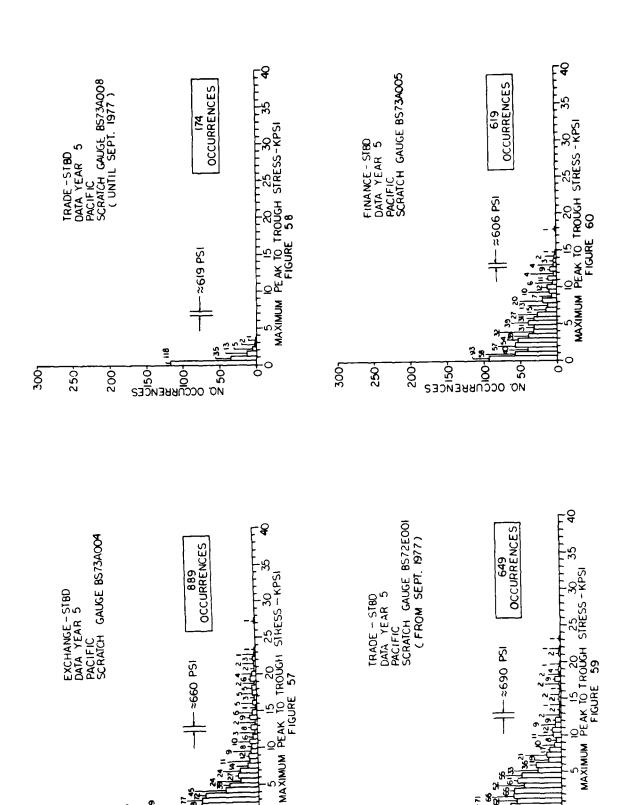






de Pantagoliano





70

NO. OCCURRENCES

3007

250-

82

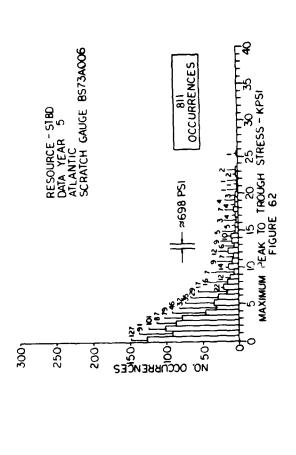
300

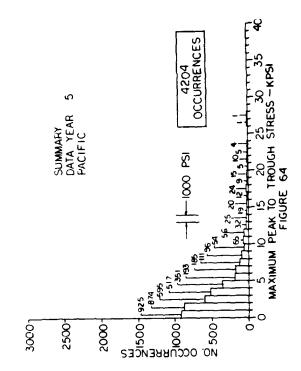
250-

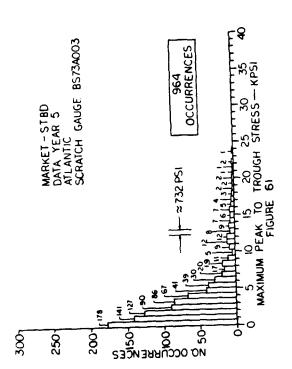
San Company of the State of the

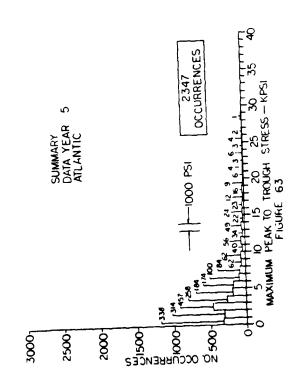
2007

NO. OCCURRENCES

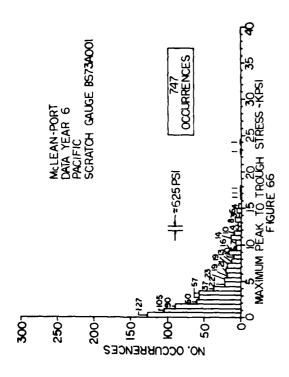


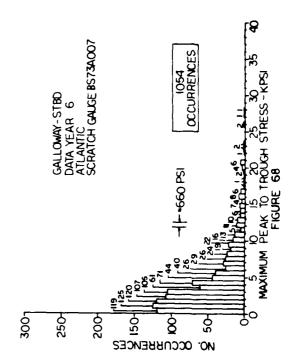


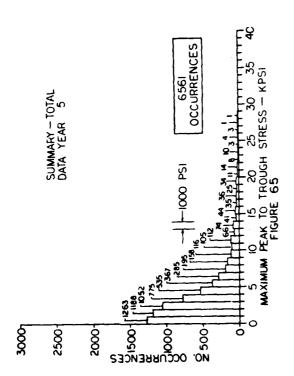


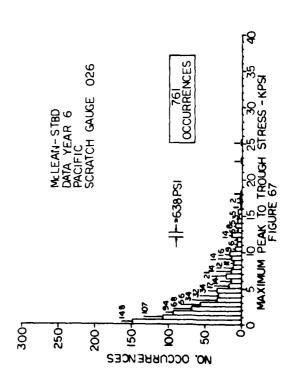


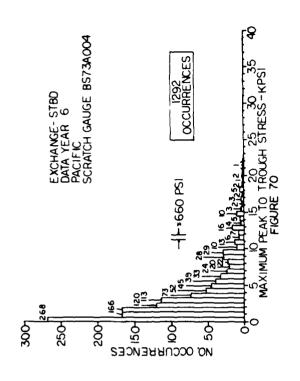
A . I Prope the street

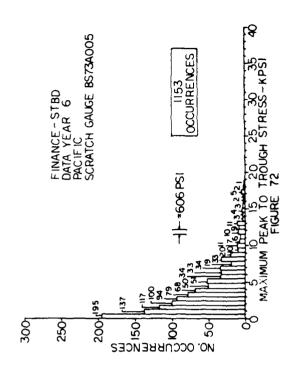


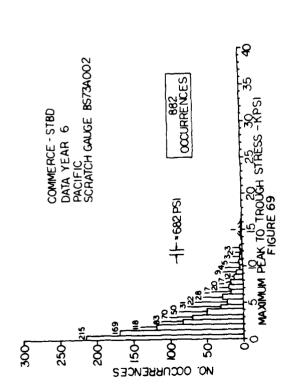


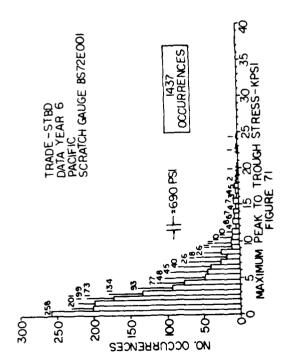




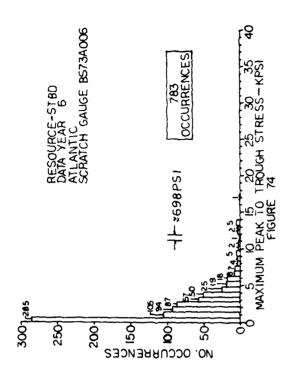


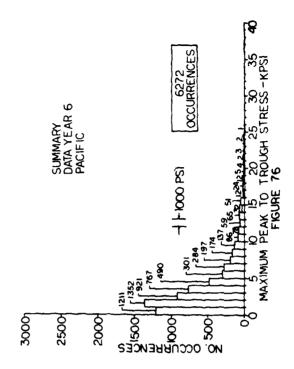


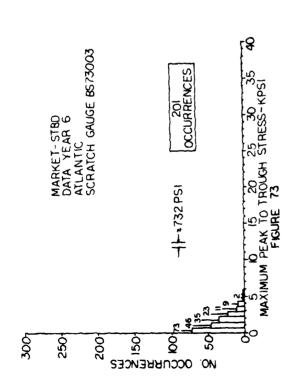


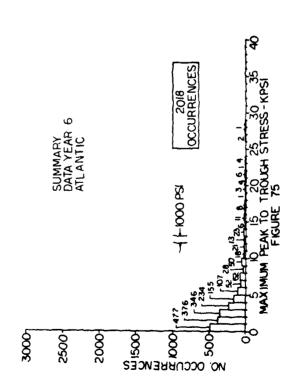


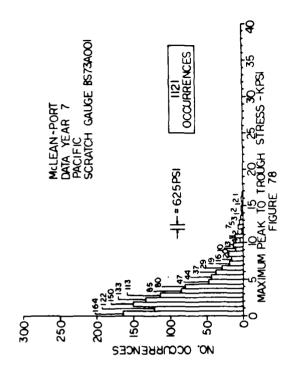
The state of the

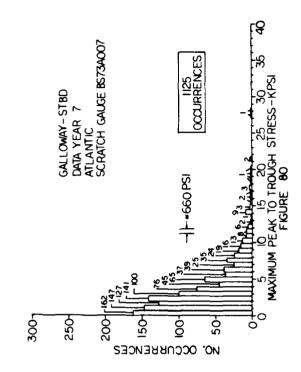


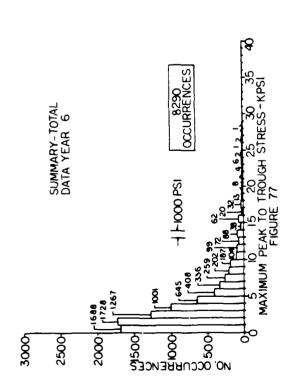


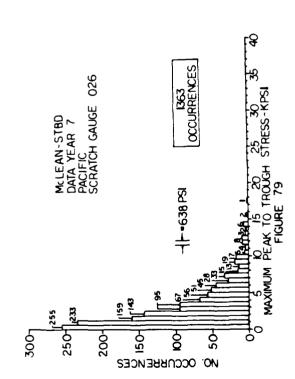


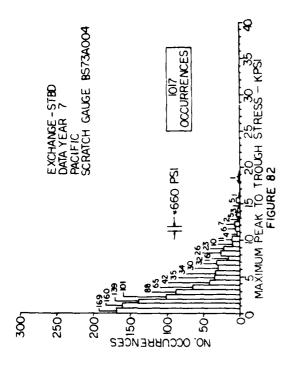


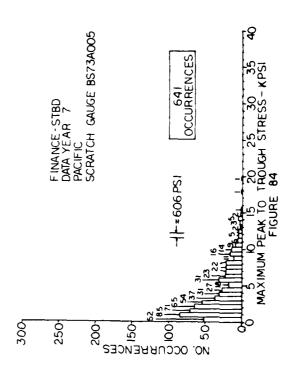


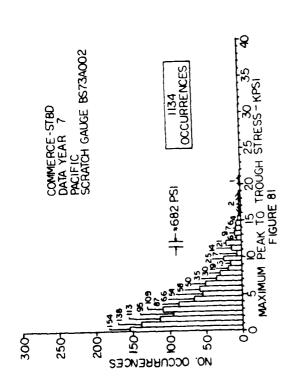


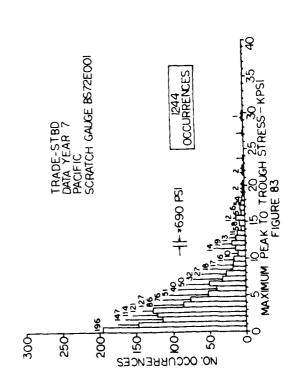


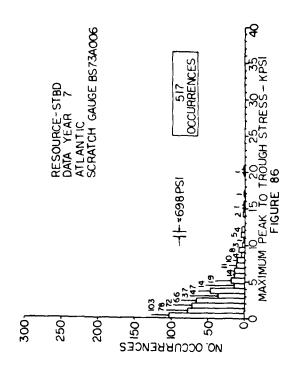


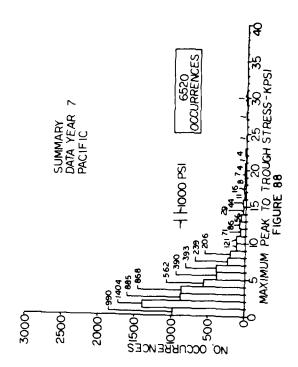


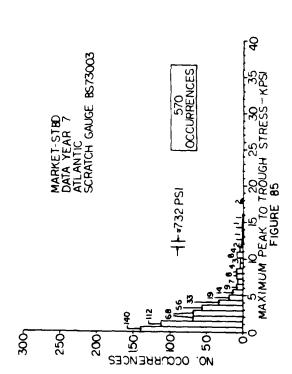


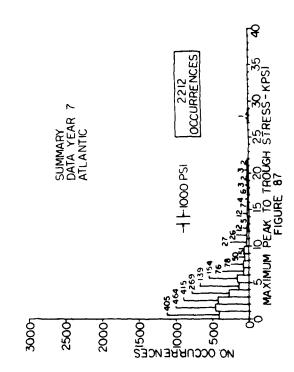


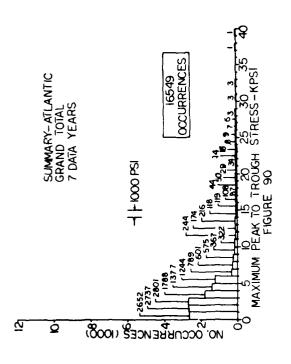


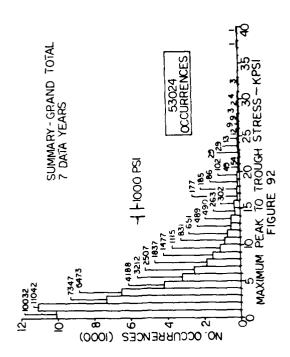


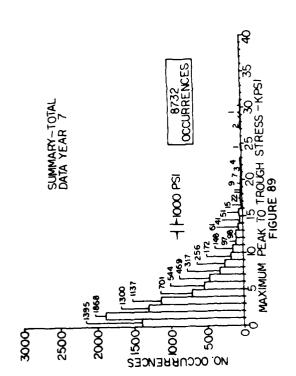


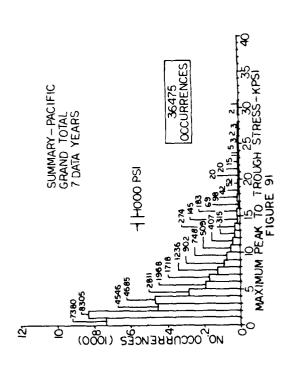












The tape-recorded stress data from the MCLEAN was recorded at tour-hour intervals. These intervals were identified by time and date, along with other notations. The scratch-gauge folders first had to be identified by the same time and date for correlation with the tape recorded data. The two arrays of stress readings were then input as data to a calculator regression analysis program with the following results:

x inputs = LVB stress  
y inputs = Scratch gage stress  

$$n = 238$$
  
 $\Sigma x = 1.413.966$   
 $\Sigma y = 1.059.543$   
 $\Sigma x^2 = 1.444668878 E10$   
 $\Sigma y^2 = 9.328.072.353$   
 $\Sigma xy = 1.10976861 E10$ 

From these quantities the following intermediate quantities were calculated:

$$S_{xx} = \sum x^2 - \frac{(\sum x)^2}{n} = 6,046,269,246$$
  
 $S_{yy} = \sum y^2 - \frac{(\sum y)^2}{n} = 4,611,133,838$   
 $S_{xy} = \sum xy - \frac{\sum x \cdot \sum y}{n} = 4,802,905,522$ 

And from these intermediate quantities the following ensues:

$$r = \frac{Sxy}{\sqrt{Sxx} \cdot Syy} = 0.91$$

$$b = \frac{Sxy}{Sxx} = 0.79$$

$$a = \hat{y} - b\hat{x} = \frac{\Sigma y}{n} = \frac{b \cdot \Sigma x}{n} = -267$$

"r" is the correlation coefficient and can vary from -1 to +1. A correlation coefficient of +1 indicates a perfect direct correlation. An r of -1 indicates a perfect inverse correlation and an r of zero indicates a complete non-correlation.

The constants a and b are used in the linear regression equation:

$$y = a + bx$$

Thus, the equation which defines the scratch-gauge variable y in terms of the LVD transducer x is:

$$y = 0.79 \times -267$$

Without using statistics. a theoretical relationship between the scratch gauge and LVB transducer can be established by determining the ratio of the distance of the two transducers from the neutral axis. The LVB transducer is mounted on the underside of the main deck. The scratch gauge is mounted four longitudinal stringers below the main deck.

Dimensions taken from the Midship Section Drawing of the ship are:

Total Depth = 19510 mm

Scratch-GaugeLocation = 2440 mm below deck

Neutral Axis = 10743 mm below deck

The Neutral Axis Dimension was provided by J. J. Henry personnel at the time of original strain gauge transducer installation in Holland.

In this case, the scratch gauge's moment arm as a proportion of the LVB transducer's moment arm is:

$$y = \frac{10743 - 2440}{10743} \times$$

$$y = 0.77 x$$

The LVB transducer was wired to record vertical bending only. The scratch gauge sees transverse and torsion stresses as well as vertical bending. It is difficult to state what effect these other stresses have on the scratch gauge excursions. However, the correlation of the statistical calculations from experimental data and the simple distance calculation is quite close, and would indicate that stresses other than pure vertical bending have little effect on scratch-gauge recordings.

The analysis presented above demonstrates that the scratch gauge on the McLean measures the extreme stresses experienced with reasonable accuracy. The other seven ships have no such independent means of verifying scratch-gauge accuracy, but by similarity, analogy, and consistency of the data, the data have every appearance of validity.

بينه خاليا شهر سور

A static calibration of the entire McLean instrumentation system was conducted in Rotterdam on April 9-10, 1973. Full particulars are published in report number SSC 263 (SL-7-7). The scratch gauges were manually advanced for each load condition and their values compared with strain gauge values. The starboard gauge is in close agreement with the Longitudinal Vertical Bending Stress Strain Gauges The port gauge also was in close agreement, with the exception of loading condition No. 1. The stress values obtained during this calibration were extremely low, varying from -1500 to +2700 psi. The changes in stress for each condition produced scratch-gauge deflections in the order of 0.02 inch or less, making accurate measurement difficult. However, the scratch-gauge values were within the expected range.

# v. DISCUSSION

Over 53,000 measurable readings of midship bending stress have been tabulated and presented in histogram form in the preceeding section. Appendix C shows a sample of the computer card listing of all the data by ship, ocean, folder number and approximate date, with the number of occurrences at each stress level. The scratch-gauge recorders, operating continuously, have also recorded numerous 4-hour intervals where no noticeable change has occurred. These intervals include such periods as time spent alongside the dock, calm weather operation, dry docking and repair layups. The scratch-gauge recorder provides a continuous bending stress history of the vessel. If the individual reducing the data from the tapes is familiar with the vessel's route and he has a known starting point on the tape, it is possible to trace the ship's movement out of port to the next port, observe the change in stress caused by loading and unloading. and the return to sea. As the ship departs a port and returns to sea, a distinct stress is recorded as the ship picks up speed. This stress is more pronounced when the ship's sea speed is over 20 knots. Recordings have been made when the vessels have gone into and out of drydock, and the static change can be easily noted. In many cases, it averages approximately 3000 psi change.

There are possibly other correlations that could be derived from this simple device, but a detailed loading distribution and the ship's log entries would be required to separate them.

In reviewing the histograms, it becomes evident that very few stress events exceed 20 kpsi. The McLean's highest stress occurred on December 19, 1973. This author was aboard at the time operating the instrumentation system. The strain gages recorded a maximum peak-to-trough stress of 53,600 psi while the port scratch gauge read 37,950 psi and the starboard scratch gauge read 32,857 psi. The ship was hove-to at the time in a Force 12 sea condition with the sea on the bow. The Galloway. Castbound earlier, was in the same storm and had a reading of 29,700 psi. The winter season of 1973-1974 was a series of heavy storms in the Atlantic. The Market also had a reading of 39,528 psi in January 1974. To return to the McLean data, the high strain reading was the result of one wave cycle occurring very rapidly. The scratch gauge, due to its mechanical operation, may not have responded fast enough to have measured the

total stress, yet the ratio is close (0.71 vs. 0.79) to the statistical relationship between the two transducers. On the SL-7 class of vessel, the ship may roll heavily and also have a corkscrew type of motion, yet the vertical bending recorded will be quite low. With the sea on the bow or stern and a low pitching motion, the vertical bending is considerably higher.

The McLean recorded high stress again in December 1977, enroute to Seattle in the Gulf of Alaska. This time the wind and sea were on the stern, approximately Force 9.

The Galloway has recorded a few high stresses during its operation. however, correlation of the ship's activity and location has not been possible. The "Mariners Weather Log" published by the Department of Commerce is a valuable tool. as ships report unusual weather conditions and log entries. For example, the Galloway reported a severe storm on September 27. 1979 but the scratch-gauge records indicate a maximum stress of only 9900 psi. At the time, she was in the North Sea approaching Bremerhaven.

The Trade reported 50-knot winds and 33-foot waves on September 27, 1979. Stress levels from the scratch gauge have three instances in the low 20 kpsi range. Again in December, 1979 the Trade experienced 29-30 kpsi stress from 60 knot winds and relatively low seas.

Severe sea and weather conditions contribute to high bending stress, but the effects can be sharply reduced by the Captain of the vessel if he can reduce speed and/or change course.

All of the original data and summaries developed for this report are available in the SL-7 data library maintained at the Waltham. Massachusetts facility of Teledyne Engineering Services.

### VI. SUMMARY

This seven-year program has been very successful in amassing a wealth of quality data. It has allowed the collection of bending data over a total of fifty-six statistical ship-years of operation. The cooperation of both vessel and port personnel on both coasts has been excellent. The scratch-gauge recorders and clocks have been removed from the vessels. Most of the units are in full operating conditions, and are available for further use.

The opinions and conclusions presented in this paper are those of the author, and not necessarily those of the Ship Structure Committee nor the United States Coast Guard.

# VII. ACKNOWLEDGEMENT

The data presented in this report could not have been collected without the interest and assistance of the crew of each SL-7. Particular thanks go to the Chief Engineer of each vessel, who provided the on-board attention these installations require. In addition, we thank the Sea-Land shore personnel who assisted in mailing the tapes and keeping us informed of vessel locations and problems.

# APPENDIX A

## SCRATCH-GAUGE INSTALLATION

# GENERAL

The installation of a scratch-gauge recording system aboard an SL-7 involves the mounting and wiring of three major components; the gauge itself, the clock assembly and the protective enclosure. With the exception of the MCLEAN, all vessels have single recorder installations located at approximately Frame 186 in the starboard longitudinal box girder (tunnel). The McLEAN has installations in both the port and starboard tunnels. Figure A-1 shows the configuration of the SL-7 class containership and the location of the scratch gauge. Figure A-2 shows the physical relationship of the recorder location to the rest of the vessel. The installation is made on the second-from-the-deck outboard longitudinal girder either at Frame 186 1/4 or 186 3/4 depending upon local interference problems.

## 2. PREPARATION

At the installation site, all components are physically placed in position and clearances checked. To ensure a minimum of effect on the vessel structure, all components are bolted to 1/4 - 20 studs which are welded to the steel with a stud welding machine. The first task is to mark all stud locations: six for the recorder,\* four for the clock assembly and eight for the enclosure assembly.

Once the stud locations are marked, each area is cleaned to bare metal with a hand-held grinder and a center punch used to mark the stud center. This ensures that when the stud is welded a clean and strong weld is achieved.

<sup>\*</sup> Although only 2 studs are required to mount the recorder, three pairs i.e., six studs were installed to provide spares in case of stud tailure during the operational life. One such failure has occurred and the quick movement of the recorder to a spare set of studs was accomplished with a minimum of data loss.

# 3. INSTALLATION (Ref. Fig. A-3)

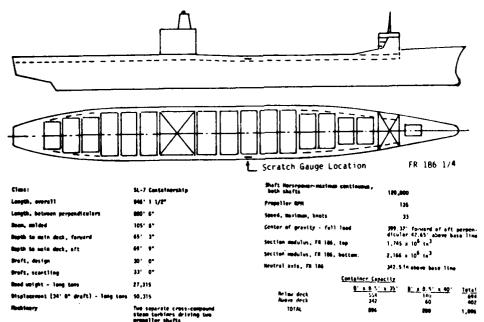
The clock assembly, the clock and its mounted plate, is bolted to the studs on the side shell. Next, the recorder is positioned and tightly secured. It is very important that the recorder studs be tight to ensure that the conical bearing points of the instrument are making good contact with the longitudinal girder.

The connecting cable from the clock to the recorder is then positioned and connected. With batteries in the clock unit, the hands are physically turned to ensure that the recorder advances at the desired 4-hour increments. When operation is satisfactory, the plexiglass enclosure (Fig. A-4) is positioned and bolted in place. Clear RTV (Room Temperature Vulcanizing) silicone rubber is then put around all edges to make a nearly watertight seal around the enclosure.

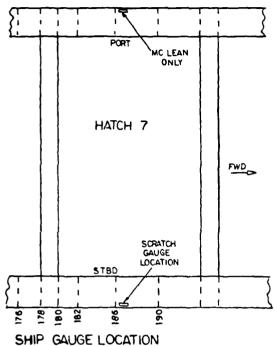
The lamp unit on the enclosure is wired to a local service of 115 V. 60 Hz, Single Phase power to operate the 40-watt lamp in the top.

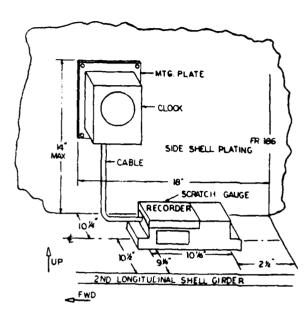
A final check of the recorder ensures free movement of the stylus arm, and proper marking pressure on the paper tape. The clock is set to GMT and the front door of the enclosure closed.

We have requested that the chief engineer mark the tape with the date at least once a week. Each roll of tape lasts approximately 3 months, at which time both the tape and clock batteries should be changed. Spare tape, batteries, and lamp are kept inside each enclosure.

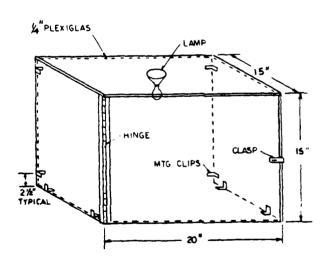


SL-7 Class Containership FIGURE A-1





GAUGE LOCATION COMPONENT LAYOUT FIGURE A- 3



SCRATCH GAUGE ENCLOSURE FIGURE A- 4

APPENDIX B

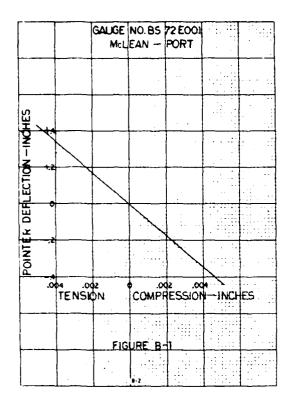
TABLE B-1

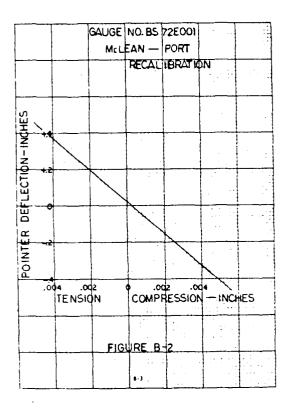
ations	inch
Scratch-Gauge Calibrations	Stylus Deflection,

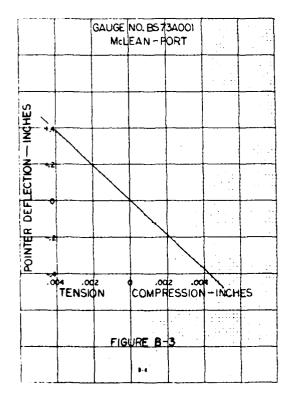
				•							
Structure Deflection inch	McLean Port (original)	McLean Port* (recal.)	McLean Port (10/18/75)	McLean Stbd	Galloway Stbd	Commerce Stad	Exchange Stod	Trade Stod	Finance Stbd	Market Stbd	Resource Stbd
0.010	0.85	0.95		0.874							
0.00	0.692	0.76		0.712					0.76	0.64	0.70
0.00	0.536	0.57	0.58	0.560	0.53	0.53	0.64	0.56	0.60	0.49	0.54
0.005	0.338	0.37	0.38	0.388	0.33	0.33	0.44	0.36	0.40	0.34	0.36
0.003	0.172	0.20	0.30	0.198	0.28 0.16	0.28 0.16	0.36 0.18	0.28	0.30 0.20	0.26	0.28 0.18
0.001			0.10		0.12	0.12	0.10	0.06	0.12	0.10	60.0
	a.a	0.0	-0.100	2.0	-0.072	-0.072	-0.08	-0.128	-0.10	-0.10	-0.08
-0.002	-0.176	-0.15	-0.20	-0.170	-0.16	-0.16	-0.18	-0.232	-0.20	-0.18	-0.16
-0.003	-0.350	-0.33	-0.37	-0.378	-0.30 -0.39	0.30 8.30 8.30	-0.36	-0.408	-0.392	-0.34	-0.33
-0.005 -0.006	-0.540	-0.53	-0.55	-0.558	-0.48	-0.51	-0.552	-0.50	6.58	-0.48 -0.48 58	-0.48
,0.00 0.008 0.008	-0.688	-0.72	-0.08	-0.716			-0.72		3	3	
-0.00 -0.010 Figure	B-1	-0.91 B-2	B-3	8-4	8-5	9-8	B-7	8-8	8-9	8-10	8-11

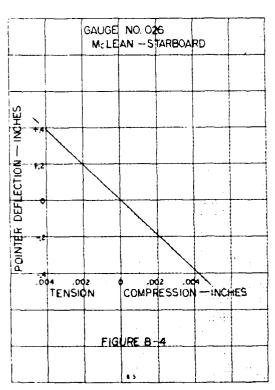
\* Installed on TRADE September 1977.

- 1 January War Stranger

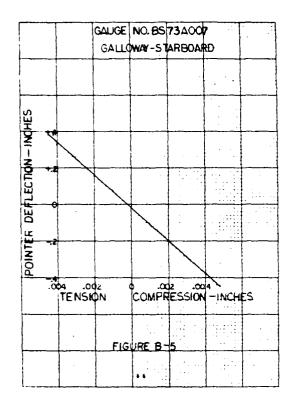


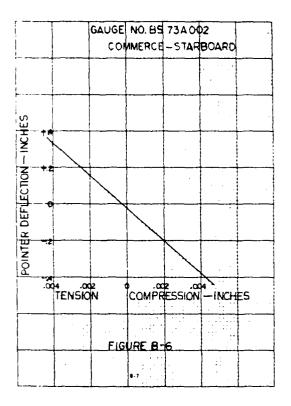


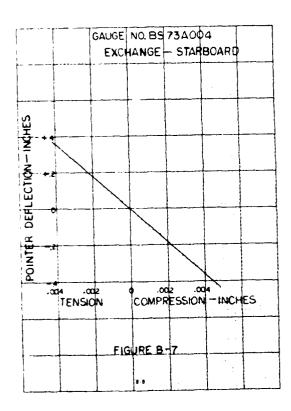


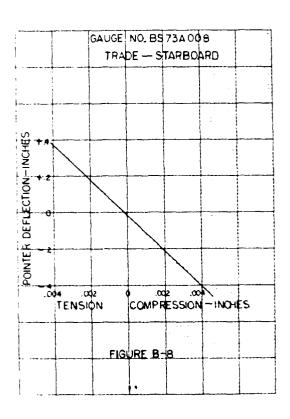


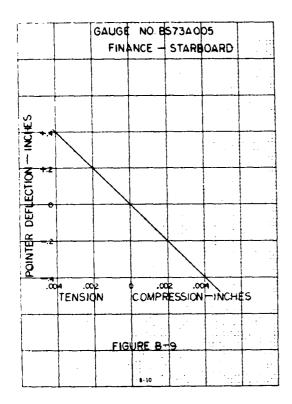
· Augustina State

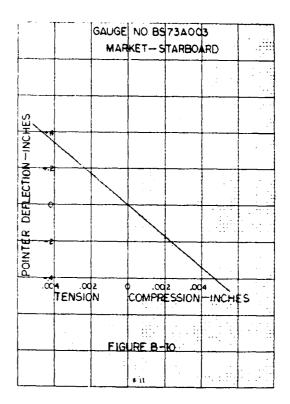


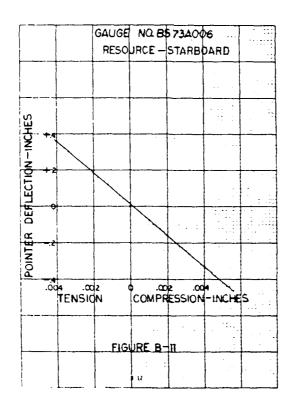












# APPENDIX C

## HISTOGRAM COMPUTER LISTING

To facilitate future use of the data presented in the histograms included in this report, all of the data have been inputted on computer cards. The data are listed by data folder. Each folder (approximately 2 weeks of data) has a header card that lists in order: the vessel name, ocean, folder number, date and data year. This card is followed by data cards that list the number of occurrences at each stress level for that folder.

This encoded data are the result of measuring the scratch length and calculating the eqivalent stress for each gage as described in Section IV, A sample of the listing is included as Figure C-1. The complete listing is available on request.

M					W= . n					
MOLEAN STAD 5 1276 F	ATEARTIC	1 10/72	3190		YEAR		_	<b>.</b>	_	
5 1276 5 MCLEAR STAR	191. 4 ATL::110	2552 2 2 10772	3176	3	4 3518 4018		5	5104	7	5742
13 628 12	127e 7	1910 7	2552	5	3190 2		ì	5702		
MOLEAN STRE	16/6 47[4:116	5 10/72=		3	YŁAR		1	31116		
A 638 13	1276 14	1914 6	2552	1	3190 2	4466				
MCLEAR STAD	4 TL A: 1 TC	4 11/72	£ 3 . c		YEAR	1				
3 638 4	1274 9	1714 11	2542	ц	3190 10	* 1929	5	unte	Q	< 104
10 5102 7	4300 K	7018 5			A 2 9 4 2					10206
2 10845 3	14035 1	165FF 1		-	•			- •		1
MCLEAN STAD	ATLABTIC	5 12/72	_		YFAR	1				
0.00										
"CLEAN STAD	ATLASTIC	h 01/73			YEAR	1				
2 438 6	1270 2	1914 2	2552	4		3878			2	5104
2 5742 3	638g 2	7:18 3	7050	Ü	H P P P P P	8932	2	9570	3	10206
2 12122 1	12760 2	13348 1	19636	1	19140					
MCLENE STALL	ATLALTIC	7 01/73			YE AR			_		
4 1276 3	1914 2	2552 4	3190	-	3624 1				3	57/12
2 63PG 3	7618 6	7656 3	F 294	7	9570 2	10209	5	13396		
MCLEAR STAL	ATLASTIC	A 02/15	3553	_	YEAR		_			_
1 478 6	1276 5	1914 3	2552	3	3190 2	3928	3, "	4456	4	5104
3 5742 4	12122 1	7018 1 1276( 1	7656		_	9570		10506	7	10606
1 11484 1 MCLFAN STAC	15155 1	9 02/73	13346	ρ	14674 1 Year	15950	1	14546	1	21692
<u>-</u>	1274. 9	1914 9	2552	1.0	3190 8		. 1	4456	4	E 1 0 0
6 57/12 2	4390 P	7656	£ - , £	10	,,,,,	16.56	1 1	4436	2	5104
MCLEAN STAG	ATLA STE	10 (3/73			YEAR	1				
7 638 4	1274 5	1914 6	2552	5	3190 2		>	4466	3	5104
1 7016 2	9570 1	10208 1			12760 1			1722r	1	-
1 21692		• -			•		•	,	•	2.0,
"CLEAR STOO	ATLASTIC	11 03/73			YEAR	1				
6 638 3	127r P	1914 2	2552	9	3190 5	5888	5	4466	4	5104
A 5712 9	ABPC 1	7018								
MCLEAR STAG	ATLANTIC	12 63/13			AF VE					
6 1276 P	1914 4	2552 4	3190	3	362d 5	4460	5	5104	3	5742
1 6390 1	F274									
"CLEAN STRIP	47644,110	13 64/73			AF VE					
9 1276 10	1 - 1 4 7	2552	319L	3	3686 1	4460	1	5104		
1912 MABUM Al 886 P	TITALITA -	14 65/75	200	41	YE WE		_			
9 638 16 1 7018 1	1276 7 4972	1914 5	2552	n	3190 4	3828	7	4466	1	43PU
MCLEAR STAD	ATLASTIC	15 66/73			AEAR					
14 638 7	-	1914 2	3628	1	4466 1	765	1	A294		
"CLEAN STAL	ATEARTIC	16 (6/73	3( )	•	YEAR		,			
13 638 4	1676 7	1914 1	2552	3	3190 1		1	5104	1	5742
1 6380 1	_ '	4932 1		_	12122 1					
MCLEAN STEL		17 (7/73		•	YEAR		••	•		
13 538 5	1274 3	1914 8	2552	1	4466					
MCLEAN STPT	ATLASTIC	14 07/73			YEAR	1				
2 648 1	1270 1	7552 1	1146	1	7618 1	4254				
MCLEAN STPI	ATLABIT	10 (11/73			YE 416					
7 636 3		1914 2	3190	1	4=66 1	5742	1	7650		
"CLEAN STRL	ATLASTIC	20 68/73			YEAR			_		
7 638 10	1276 4	1914 #	2552	3	3196 1	3658	5	5144	7	E742
2 6380 1	7617									
MOLEAN STAD	ATLANTIC		366-	_	YEAR			n 6	_	
7 638 11 1 7018	1276 4	1914 4	25"2	7	3190 4	2628	3	4466	1	5104
MCLEAN STAG	ATLASTIC	22 .4/13	- ii Q / 7 1		4674	1				
6 A38 4		2552 2			5104 1		1	7016		p 2 <b>c</b> 4
1 11484 1		10074		•	, , , , ,	1146	1	,016	ı	~ ( ~ 4
1 1 1 4 4 4 1	15140	1 -0 -								

# APPENDIX D

## DATA AVERAGES

As required by the contract for the final portion of the scratch-gauge project, the top and bottom of each four-hour scratch mark on the data tape was measured from a reference line. The numerical average of each scratch was then calculated. The purpose of this calculation was to determine if it was possible to read diurnal stress or other static changes from the scratch-gauge records.

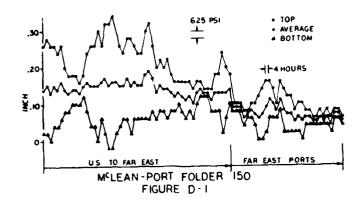
The measurements made were encoded on computer punch cards. A listing of these is presented in this Appendix. Each folder of data consists of a header card listing the vessel, ocean, folder number, date and data year, followed by data cards with Bottom-Top readings in hundredths of an inch (reading horizontally).

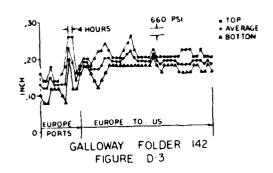
Although all the data are shown in the listing, only one folder of each ship's scratch gauge data is plotted and included here.

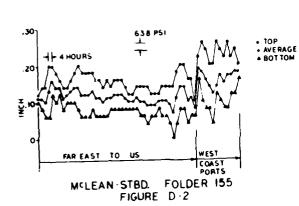
Each data point represents the four-hour extreme stress experienced underway with the time in port excluded. Each plot is divided into an ocean crossing portion, and time spent between ports, with all data in correct time sequence.

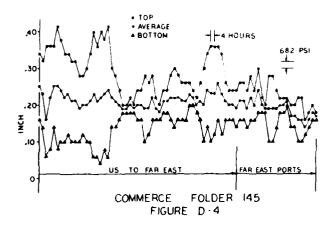
With the exception of the <u>Market</u> and <u>Resource</u> plots, the average stress change compared to peak-to-trough maximum stress during ocean crossings is quite low. There is no evidence of diurnal stress on any of the plots. On the McLean and Galloway plots and all of the others to some extent, there is evidence of bias to one side. This is shown as a repeated lower or upper reading regardless of the length of the total scratch excursion. The only explanation that I can conceive is that while at sea these vessels present a large sail-area to the wind and tend to sail with a constant list. This phenomenon is also observed in the ships roll where the roll to the windward is much less and more constant than the opposite roll. In reviewing expanded oscillograph records of McLean Bending Stress Data, the same bias was observable.

The trim of these constant-draft vessels is important, and as a result the crew monitor the fuel consumption and ballast conditions, and adjust them as required a minimum of twice a day and more often as required. This constant trim keeping would result in the small change of average stress evidenced by the data.

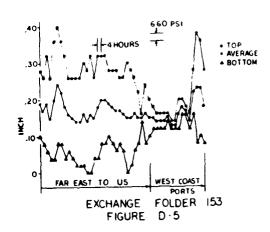


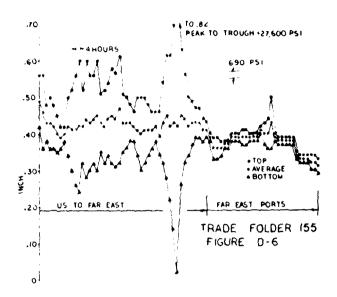


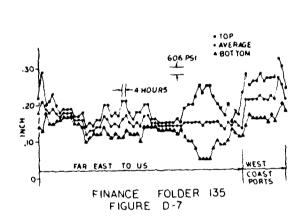


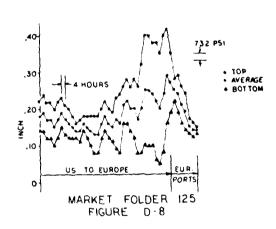


· Sandania Comment

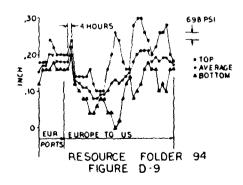








· number



"CIFA"		•	FACTET	C 14	12 11	179		45 46	. 1						
50	2 14	2.2		2.2	ا. تر	22	24	۲ ۾		25	٧		_		
٦٢	7	26	٠, ٢	2+	نر ج	24	14	يا خ	ج ت	54	3.2	21	24	20	7 P
4 نے	3.0	è t	10	77	3,7	5.6	38	25	10		3,,	29	33	24	نے 1
۵ ۵	30	ا، تے	ر ۲	20	3 c	18	32	į A	31	20 14	اد <b>ب</b>	21	35	54	56
12	3.0	1 +	۲,	16	32	16	3,0	្នំឧ	32		t a	3.5	136	14	10
1.0	۶۵	1/4	₹.,	ρ	T #	10	a c	16	32	16	3,7	1.5	3 8	17	29
م ح	ح ۶	1 6	ج ۲	ا بر	11	ہ ج	32	23		15	و ۾	1.2	3 e	12	36
۾ ج	<b>4</b> (1)	ź A		26	نے ۲	26	12		3.1	24		20	5 b	24	34
24	تر ۽	22		21	4.3	ĹĀ	3 t	24	7 (1	2"	3 -	50	30	24	3 A
16	416	1 6	3.6	1.0	36	ρ	44	1A	3.2	16	34	7.5	3е	1.0	ح را
2.4	32			•	•		4 4	4	цр	٠	40	ρ	"c	16	3.0
"CLF AA	C STOP		PACTET	Ċ,	<b>3</b> 1 -	-11/7	c	W. L. 1.							
1 4	۶۶	18	۶،۰	14	Fà	2 n	ີ <b>ວ</b> ວ	YEAR							
1 ^	24	A	*, <b>F</b>	٠,	3 7	4	¥ #	14	1 "	14	1 4	14	20	12	26
я	Ç ri	د ۱	۲,	12	32	10	14	12	40	15	3.4	17	46	10	36
1 ^	به د	1 %	ړ د	10	ر. څ	14	70	12	32	1.5	> n	1 4	25	ą p	32
1.4	1.8		ŕ	•		, ,	7.	14	55	1 1	ટે લ	ح 1	٤١	14	20
"(trai	STAP		FACTET	. 1.		179			_						
٨٩	30	20	ج ۽	27	<b>.</b> .	28	> "	AFVE							
22	26	22	ودح	ž i	12	55	34	20	20	24	20	211	26	22	24
20	₹#	68	1 1	20		22	7.	7.0	10	r',	<b>1</b> (c)	21,	30	20	44
22	44.47	22	بخ 🛪	ć 6	3.7		3.3	اد نم	3,4	1 2	0.5	1 4	51	12	44
23	60	24	4.1	2.5	3 C	66	3.0	56	3	24	35	ĩ /.	30	22	40
23	26	52	₹ 2:	ء ج د ج	36	م در ۱۰	3.6	50	f1 -4	62	"?	1.8	44	2 ^	38
22	3.1	Į A	10	[ ]	už	26	3.0	5.9	3.3	57	3.4	20	3 4	24	3.2
"CLEAS	3150					16	40	50	3.8	ž "	ح ي	24	2€	-	
24	26	26	T-,	23	- 4	-12170		AFVB	7						
2 a	ح)	٠١ نے	٤,,			5.5	55	2.1	32	1.5	36	50	۶٤	211	30
ود	ية خ	دڅ	24	11	7.4		9.9	1.4	3.4	1.6	34	12	20	۸خ	51
ہ ج	برد	14	20	50	26	20	20	<i>-</i> 0	5 1	۶۶	24	27	24	۱۱ م	26
۰ ج	ا د	į n	2.5		24	4 [	72	1 +	23	10	P 4.	} <b>~</b>	24	ہ ج'	ي ج
14	20			10	ر) خ	j p	25	٠، ح	55	1 14	<b>2</b> i	1 8	22	ĨÄ	55
METTAL	STOR		ج. 13ء جا 1	10								-		•	٤ و
12	<b>\$</b> \t	19	141, 14 13, 13					44.48	7						
16	۸ در	1 4		10	20	14	ن د	1/1	ء ر	14	3.	16	20	3.6	85
16	26	, a	2.:	14	2 ~	16	ع ج	1 6	ن ۾	16	20	) A	20	14	26
16	24	24	20	Į A	26	5.0	3.	1 14	36	1 4	1	16	36	16	26
2 ^	(4	i A	۰, فر	F 1	ē۴	26	ع ح	۲ ۶	24	20	20	جخ	36	50	35
"CLEAN	STHD		21;	22	7	ج ج	₹6	ی ج	26			• •	76	£ ··	3.6
24	7 ii	äh	1. ACTS 16	1.47		73-03		AFVE	1						
1 A	324	14		26	۶ نر م	2"	30	12	3.2	27	3.5	20	34	1 4	40
20		£ 0	4.	۸ در	c. i	į H	בן ני	14	46	1.0	40	į e	30	59	42
21	4 E	211	ek er	50	4 (	1 14	š 12	50	30	25	3 6	دن	3.	ہ ج	34
, h	<b>4</b> 0		در ۲	<i>2</i> K	2 v	2.0	3.0	26	30	20	3.	6.6	3 (	۶.	30
22	ξ2	ĉħ,		2 8	<u> </u>	26	ع ج	2.1	3.2	22	10	ž e	5 e	ح کے	10
ار د	3,	دم م اد:	¥.,;	7.7	? 6	20	36	د ن	3/4	2.5	3.4	28	30	د ج	
*{ + + A+.	371.0	الانح	20	₹#	36	64	₹ ;	64	26				, -	6 -	36
ه نه	15 8	32	ACTI TO	148	•			YFAG	7						
32	رو. ام را		٠,٠	2.9	دڙ	30	51	r R	4.8	ĉ h	<b>E</b> (1	34	نع زن	7.4	
12	18	12	86	4.4	45	14	32	3.0	110	36	44	34	46	34	5.2
32		3,2	E ()	32	4 t-	3.5	₫ 6	30	<b>8</b> 54	30	9.4	38		3 %	46
	12	\$A	15 6	36	45	34	4 2	3,2	44	جَوَ	n g	35	46	34	44
1) 30	ائر () در با	50	11.75	311	46	34	4 ċ	30	4.2	24	ڔٛۼ	3 C 3 O	5 č	32	ڊ <u>ن</u>
40	48	14	<b>3</b> /2	42	5.4	36	٩,	50	<b>લ</b> ોં	ج ہ	56	411	13 per	37	4R
	45	40	44.	3 4	43.	38	0.9	3 11	112	34	4.1		44.	3.4	<i>1.</i> 14
3 1	110	34	11 Z	14	40	50	16	ŝа	46	3,	د د. ح د	36	20	3 4	14.44
3.6	50	12	< :.	34	· A	36	4e	£14	4.4	36	£ }	4.5	• 6	3.0	$n_{A}$
32	V-5	3/1	5.,	3.8	1.7	36	84	js	42	35 40		30	60	34	64
34	46	3 4	K. 1.	32	4%	31	ωė	ฐี¤	a P	33	44	3 14	74	3.4	46
34	48	24	1. 1	( a	60	60	e 6.	, a	56	28	5 ,	30	54	3 (1	50
ΑÇ	SH	è P	K (,	42	<b>t.</b> ,	3 11	15 (5)	30	13.	34		۽ ۾	5 U	30	F 2
								<b>-</b>	• •	3 "	44	3+	44	34	4 G

48	4.5	36	4.0	42	42										
MCLEAR	3740		CTETE	1.13	1 - 2	2/60		YEAR	,						
20	25	20	22	20	رج	16	2.1	1.4	24	14	24	1 8	2,	16	26
10	2.	10	3.2	14	Ž.	16	26	16	24	14	3.0	14	يَ دُ	16	-
20	55	e (	2	12	21		76	,6	10	16	7 4	16	ک ر		20
	24	18	54	16	24	1 6	24					-		1 A	2 %
16				-		-		50	24	1 1	22	<i>i</i> '	24	55	24
1 /1	1 8	1 1	24	14	20	12	54	1 4	3.5	1"	<u>2</u> c	15	2,	14	2 1
12	۱. د	10	2 5	P	26	P	غد	6	26	<u>^</u>	3.,	10	3 L	1 ^	24
10	25	12	24	10	22	1.6	28	16	32	15	3 11	14	2 c	1 6	26
1 //	25														
MCLFAP	ن ۱۰۰ ت	FA	CTFIC	15°	رح،	/ P C		YEAR	7						
20	3.2	ė o	47	16	<b>7</b> . (-)	14	5.5	16	24	16	26	20	24	20	24
۷ ح	ント	1 14	21	16	2 14	1.4	۶.	20	24	20	24	20	26	- A	30
u	42	А	12	1 2	34	1.4	32	į A	3.0	22	28	ی نے	30	1 A	30
1 8	26	20	8.0	22	42	14	44	0 \$	40	16	ر به	24	3 1:	ہ ئے	36
ż۸	3.6	1.8	24	20	3.2	1.8	32	1.4	3.4	16	3.8	16	34	10	
12	45	ż٩	14	20	٩ς	¿ 0	26	20	20	-				-	40
	28	20		_						2 C	5 4		20	55	24
45			26	14	-	10	4.8	h	40	1.6	ح ں	10	ជរ		
MCLEN	STED		CTLIC	151	0.37			YEAR	7						
20	40	16	3.5	12	0.4	P	50	10	4.3	16	u .,	10	41.	12	14.74
4	4.0	10	T ja	1 ^	3 7-	10	3 7	lv	3 C	10	30	14	44	6	ج ۽
>	5.8	4	۲, ۱	A	ii b	æ	41 C	12	34	5.4	3.5	26	32	24	2.8
Į A	26	16	2.0	1.4	1 6										
MOLEAN	STED	PA	CIFIC	152	U 3 /	/ A +)		YEAR	1						
15	26	14	24	14	22	16	24	16	20	1 8	25	Į A	2 c	1 6	24
20	24	18	20	16	20	14	30	10	24	<b>1</b> a	3,2	À	36	14	3.4
10	40	4	ح ال	4	42	5	3.6	и	12	٠,	ر و	4	54	,,,	44
,	48	6	3.0	6	<u> </u>	F	48	u.	38	0	40	Ċ	40	ŋ	116
ń	0.8	n	40	,	14	À	44	4	34	10	3 14	10	3 c	10	
10	28	15	ر ۲	12	è c	14	26	•	34	1,	3 /4	1 (	36	1 '	50
MCIEAN.	STEE		CTETC			/ P D	76	V.C.A.C							
				153	<b>&gt;</b> ()	-	~	YEAR	7				• .		
1.2	25	16	20	1/4		14	2 C	16	18	16	24	1 4	24	18	25
1.6	<b>2</b> (	16	20	50	26	50	20	ر، ح	>6	20	ਟੇਲ	<i>ڪ</i> 11	يد تم	50	26
1 1	11.6	16	3.5	1.9	24	1.6	9.6								
"CLEAR	STAD		CTFIC	154	64,			YEAR	1						
۵ م	50	āh	4.4	ž A	0+	م ج	46	30	45	30	42	3.5	46	3.0	40
32	38	15	₹ -	32	3.5	32	36	2 8	9.4	24	44	24	56	24	5.2
211	16	1 8	a a	12	50	20	5.6	2.5	50	2.4	42	26	44	28	4.4
2 4	46	۾ ج	11.4	۾ ح	a G	50	02	26	46	23	ج آ	30	44	30	4.0
32	0.0	3.5	4 (.	<u>3</u> n	45	30	40	54	4 0	37	1 A	34	3+	31	٦,
34	3.4	3.0	10	3.6	410	36	40	36	30	3.1	٦,	32	40	50	44
2.4	46	Ža	<b>c</b> 9	2 A	E (*	į A	9.4	30	36	30	٦,٠	3°)	3 0	22	34
24	ЙĠ	ē 1.	24	24	<b>2</b> (	 b	3.0	26	4 O	5-	٠.5		30	28	30
45	11.5	24			2 12	24		54	31			c+		_	
د کے	7 P	20	4	2.1		۶4	30	84	31.	22	24	64	≥ 6.	24	5.5
MCL FAR.	STED		TG CT+TC	27	76 	/ O ::		41.40	,						
			-	155				YEAR					_		_
30	3.2	45	1.4	26	<b>4</b> (4	26	4.3	4,2	40	3 (:	3 9	32	36	a 5	34
30	34	3.0	4.6	30	3 12	28	44	_	37	36	39	54	30	2 p	3.4
54	\$ m	22	16	24	₹ ()	èь	30	۵۲	¥ 14	28	36	c p	30	ĉΑ	60
<b>8</b>	3.4	ć <sup>14</sup>	12	5 11	3.2	2 B	3.4	26	34	26	34	20	34	26	32
54	32	2 A	۲,۶	7 h	8 11	24	34	24	3.4	50	3.4	€4	30	5.6	49
۾ ح	4 ቦ	211	36	71	71,	26	٦,,	36	4.5	51	45	٦P	44	ЯÇ	4 O
5.0	4.6	32	11.65	50	11.4	è P	47	۶,۶	46	37	42	32	40	34	54.
MCEFAN	STAD	FA	01110	156	٠ 5 ،	/ P 👌		YFAS	7		-	-		-	
3 0	440	36	44	30	e 🛬	3.0	54	50	5.4	32	κ,	g n	56	50	٠ (
34	5 ()	3 14	46	Į p	<b>E</b> (	ζp	خ ۽	36	ج ک	51	5,6	36	5.	411	نغ 11
34	34	36	ŧμ	34	3.6	30	a Ž	30	44	ر خ د	44	م و	46	32	4
34	114	34	// 2	5 2	46	34	11.2	3 () \$ A	40	36					112
36	44	34	ج <i>ہ</i>	40	4.4	36	υ. υ.				40	36	40	34	
34	40	36		7 A	4-			36	यु स १८	36	42	g A	دائل مار	34	46
	40	30	य व			36	4.5	3 n	36	ر ب	3.4	36	"(	34	n Ç
30	73.17	٠٠ د	45	<b>5</b> n	11.14	15	H C	3.0	49	3 6	<b>4 %</b>	34	3.6	a S	46

ח כ	40	30	16	30	32										
MELFAN	STAR		OTETO	157	15/	P.J		YEAR	7						
۾ح	7.4	24	16	أاغ	4.5	26	3.5	26	30	20	τ,	م پر	34	ρA	ج ،
ه خ	12	24	10	à	34	28	3.0	56	34	è 4	36	3.	5 c	24	۲.,
2 n	خ۶	2 h	7,7	ء بر	<b>1</b> ()	2h	۽ ح	24	نَهُ حُ	52	2 4	ں ج	26	٦٤	2 6
45	<b>5</b> ()	c A	Ψij	۽ ۾	3.0	الغ	3.	۾ ج	30	بے د <i>ا</i> نے	3 .	36	26	30	
"CLEAS	STOP		ECTETL	144	00/			YF AP	7	κ,	ر، د	7. 4	1. 0	.3	3.5
30	ેરટ	32	10	2 h	31.	ភ្នំគ	٦ خ	۾ خ	132	26	14	ċ4	3 H	24	با ح
ه ج	30	۵.		r ···	•	•	_	r	- 6	, ,	4	ζ.	. •	۲.	~ "
MC1.F x+	קשופ	۲	SETFIC	159	06/	A iv		YEAR	,						
۾ ج	10	3.0	3,	30	44	32	36	52	36	3.1	36	37	34	2.3	3
32	34	2 2	<b>3</b> 1	3 m	۲,	45	34	۾ ج	34	۲۶	υ <sub>1</sub> ,	24 24	// c	32	34
2/1	35	, a	1	8	7,2	30	32	32	3.4	32	34	32		2 "	44
۾ خ	30	ćρ	3.0	۾ ج	1	۾ ج	30	3 6	3.4	11	7.44	3 6	34	3 n	2.4
"ELFAI	STAD		NOTETO	160			3 (	YEAR	7						
-	2 (i	16	111	12	20	12	2.5	4	<b>' 3</b> .3		2 .	• 0	٦.		٠.
16	18	14		10	20		2.5				3	1.0	26	12	20
16			ن ج •			16	72	16	5.5	15	2 (1	1 *	1 7	16	20
16	16	16	1 /	16	1 14	16	3.8	16	1.8	1 14	2 (:	1 0	Šι	1 8	5 ú
18	20	18	2)	1 8	20	1 5	20	20	۵۹	1 2	2.	1 *	21	1.8	20
م ر	20	18	<b>2</b> ()	16	ن ج	16	2 C	16	50	14	ē (	1 ~	25	1.4	24
1 /1	20	14	20	12	با <b>ج</b>	12	20	15	20	14	211	14	50	1/4	20
14	20	16	( p	16	1 6	1.8	> C	18	50	t H	€0	I b	20	16	55
1.6	2.1	14	28		_										
"CLEAR	STEO		4C 14 1C	101	ر7 ر		_	ALVE	7	_	_				
12	<b>3</b> (1	12	* ()	16	26	14	56	1 2	5 4	1 n	55	1 12	2 ĉ	۵۸	22
٥ ح	25	1 14	25	1.8	2.5	٠,	24	50	2.4	1 12	25	1 2	ے کے	1 12	50
1 0	25	1 8	2.5	l u	ح ج	н	Pζ	n	5 %	6	26	44	20	4	16
A	ب د	r)	24	>	25	5	2.4	7	5.4	•	1 14	14	10	16	18
1.4	1 7	12	1/4	12	1 a										
"CLEAS	310°		ACT+ IC	102	047			A L V V							
1 (*	1 4	12	1.4	17	12	8	12	ح	14	А	12	۴	12	6	12
1 ^	1 6	10	16	a	1 1	£	1 1	(13	10	12	<b>ا</b> ح 1	1 //	10	1/4	10
1.4	16	15	1/4	12	16	16	٦ ۾	1 4	2.5	10	₽,	12	2 ċ	14	20
16	16	16	1 12	1 6	4 1/1	16	18	16	1 24	16	16	12	14	17	14
a	10	*	1 🗡	1 6	1 1	1/4	5.3	1.4	16	15	1.6	5 1,	26		
"CLF A"	STEP	P.	ACTETC	163	QH/	1 K G		AFVE	7						
۱p	され	20	26	: 1	<b>2</b> 11	50	24	24	26	1 5	20	27	یہ جے	22	214
22	24	22	21	5.5	24	4	30	16	3.3	1/2	2.6	(۱ نے	30	م ح	26
12	26	62	2.	22	24	6.2	24	22	٦. ٢	211	26	35	24	22	24
22	24	1 8	<b>T</b> (:	1 4	20	è 5	26	ح ج	2 11	22	7.1	22	ي ح	20	211
20	25	1 ts	25	1 2	2 4	61	24	22	24	20	2.2	20	21	1 🖴	20
1 =	<b>?</b> (:	1 10	2:	1.2	20	1.5	20	<b>1</b> 12	20	1 2	2.5	15	24	1 8	52
101.8 41	STICE	μ	10 1 F T (,	164	697	170 11		48.34	1						
1 6	20	16	26	1.4	2 ~	1.4	3 2	12	٠,	12	34	12	30	12	3.2
j s	28	۱ ۲	<b>2</b> B	1 4	2.4	1 5	24	1 4	3.,	i u	20	1.6	24	16	2.2
16	ب د	20	22	14	خ ل	10	1 4	1.8	۾ ۾	12	14	12	16	•	
MELFar	3.7 H/N	£.	ACTETO	165	(0)	1 5 6		Y (; A fe	,						
1 ^	1 2	10	12	а	17	10	12	10	12	1 C	10	10	۱ä	H	12
£ £	1 (	ρ	1 0	1.6	12	1.4	1.8	16	1 4	16	15	1 6	2 (.	16	2 เ
16	25	16	20	1/4	20	16	23	16	<b>2</b> (	į p	2.,			•	
"CLEA"	FURT	F.	ACTFIC	130	1.47	177		YEAR	1	-					
24	4.2	22	1,	211	3.0	2.5	2.5	5.0	31	24	3.2	22	٦,	2 n	32
20	1,2	20	1 1	جج	32	ح د	20	ء خ	ني	45	3 4	64	3 c	۱. م	30
24	45	24	311	22	3 (;	جير	35	ي ج	5.4	ہ، خ	30	ں ج	n.	ه ج	3,9
ر د	40	24	٤,.	2.3	30	6.4	10	21	30	2 5	3.0	4 4	ξ.,	مو ئے مو	10
وَمَ	36	25	1 4	الأفي	10	20	7 ,	22	16	ر خ	18	ê n	34	ءَ جُ	16
۾ ڄ	ΛU	ار نے	3 8	د خ	رالة	٦څ	9.0	14	50	16	ج ع	16	42	1 P	<b>~</b> 0
14	50	1 P	13.4	م م	1,6	5.0	n a	26	44	52	4.1	24	3+	54	36
رر فے	34	e 4	7.4	30	33.	30	36	מק	12	45	34	26	34	32	40
5 ^	40	, a	36	24.	ĩ.	٠٠	12	ا ج	<b>\$</b> 0	5 h	3,4	ج ج	3 e	5 N	26
مخ	36	į A	8 H	ەر خ	نہ ن	26	46	خ ج	12	50	36	12	વક	6	114
•	,	•		•	*.		- 1.	٠,	•		26	1 E	- 6	r,	-1 [

* 56	10 54	2 r	42	26	" L	26	10	28	34	24	34	28	12
HELFAR BURT	PACTATO	140	10	-11/79	1	AFVB	1						
24 30	AC 55	22	3 (,	٥٤	24	ہ ہے	2.5	20	26	5.5	74	22	26
22 26	22 24	22	7.4	54	26	24	26	22	24	2.4	26	24	2,5
26 26	20 24	ė 0	53	55	2.1	55	ي ج	25	۶.,	جرج	24	20	ر, د
24 74	20 24	ã٥	26	20	24	14	٤٤	21	نےخ	15	2	1 A	
14 24	12 21	12	3 C	ħ	30	. 4	24	۾	٣٩		ی د	-	24
nn 26	ű 24	Á	3 5	6	₹,	10	ર્ફ તે	10	26	10		4	× ج
14 26	14 20	12	26	14	24	14	24	15		•	ب <i>ح</i>	12	20
•	מב מב	ξź	38	20					ž t	16	ې د	1 *	26
•		27	<b>7</b> C	<b>6</b> 1)	30	55	3 v	20	30	50	2 r	22	24
				470			_						
MCLEAN BURT	FACTI 10			179	_	YEAR			_				
55 45	66 th	SH	3,0	26	34	č.h	32	36	3.5	26	32	211	12
211 72	en Tu	à h	10	24	34	2.5	3 4	۲۶	34	55	2¢	50	3 #
≥n 40	50 00	5.0	18	50	38	50	3 е	70	36	14	40	10	56
12 48	16 de	5.0	18	55	36	24	38	8.5	3.6	2 <sup>p</sup>	34	45	34
ع ع ع	26 34	24	38	24	a (	24	40	2 č	$u_{10}$	<b>2</b> 0	40	50	46
77 44	1411 65	22	44	5.5	Hij	24	3,8	56	36	26	34	22	3.6
23 کرچ	20 x4	رږ	1.2	22	34	جج	3 4	Ž(,	3,6	20	40	52	3.0
20 42	53 55	211	3.0			-	•	-		, ,	•	Ę.	, •
MCLEAR FORT	PACTETO			-12/79	3	VEAR	7						
22 36	14 5,	16	84	5.5	36	20	30	24	28	22	24	3.0	•
18 38	20 TH	52	38	50	25	26	2 d					50	34
•		50		20				5 0	36	14	44	50	7.5
•			34		30	۲۶	30	22	۱, ت	5 c	2+	55	26
28	45 05	2.0	3.2	5.0	30	60	24	2.5	٦ć	22	3.0	50	26
22 24	10 1	5.0	30	40	26	50	ن <i>ج</i>	20	80	55	3 u	50	30
50 ga	25 28	27	\$ C	<b>S</b> S	3	0 نے	46	20	30	16	34	16	34
10 38	10 46	12	44	15	14 C								
ማርኒክላክ የጦላቸ	PACIFIC	143	15	/79		YEAR	7						
18 37	1# 10	16	30	16	3 2	10	34	16	29	16	36	1 8	32
54 45	CD 35	1 8	16	r 0	34	20	32	211	12	22	34	21	3.5
18 32	20 32	12	31.	24	26	24	5.4	24	34	22	54	جج	34
22 34	in in	24	ţμ	5.4	35	26	30	26	32	ŽΑ	30	25	30
211 24	77 24	24	34	۾ ۾	36	۾خ	3.0	26	12	-		• ,	, <b>v</b>
MELENY FORT	PACTETO		12	179-01		YEAH	,	-					
20 36	in in	2.0	3,7	24	3.5	الم نم	3.5	25	u լ	24	40	22	112
20 02	20 44	ຂູ່ຄ	42	50	4 C	50	40	20	112	18		_	
jn 40	18 38	16	30	ćū	36	_	3,4	18	_	-	46	16	25
•	•					16			36	24	36	24	32
<del>-</del>		ار نے م	32	24	3 C	54	30	24	3.2	<u>e</u> 6	36	26	12
24 12	211 30	56	36	26	36	5 11	36	2 F	7 0	56	36	30	4 C
42 48	32 46			1									
MULEY' BUEL	PACTETO		1/		_	AFAB	1						
90 30	हैं। रह	۾ تے	₹ (*	2.2	30	ح د	24	53	12	2.0	30	16	46
14 30	16 34	B	37	C	57	Ċ	52	1 (*	G(A)	54:	45	18	40
12 44	12 0.1	12	u A	15	نے نا	1 14	10	10	30	16	30	14	40
14 30	50 x5	20	3.2	è 11	ع ?	5 7	26	5.5	3.5	2.5	20	٦٠	26
22 42	50 x2	م ج	2 1;	15	3,19	12	4 C	12	34	12	30	12	40
12 40	10 11	() نے	20	22	35	٦1.	30	16	34			- '	
MCLEAR HIRET	PACTETE			2120		YEAR		•					
10 24	14 26	16	28	24	32	ž4	30	ه ج	3.5	24	36	24	33
20 25	26 30	26	28	ĬP	24	į A	24	را نے	26	ہ ج	ہ ج	חק	24
18 26	20 28	16	26	Ž٥	76	16	2 €			_	_	-	
14 26	16 26	16	24	16	5 1			16	26	16	2 u	16	24
-	•					16	20	16	26	2 °	<b>?</b> €	16	28
·	•	16	30	16	36	41	30	Į p	30	16	54	1 4	1)
20 30	18 4	50	2 B	50	<b>,</b> C	50	30	50	28	50	30	Su	30
#5 75 Males 05/17	50 26	22	76	22	24		_						
MELLAN, PERT	FACTETC			110		HV 4A							
22 24	P 59	4	40	15	38	1.0	45	16	" 0	5.0	311	5.5	36
5u 5A	18 49	1 P	36	2 (1	2₽	24	40	16	40	ē4	36	518	3.8
511 34	82 34	50	3.6	50	32	24	35	26	3 4	<b>2</b> ()	36	50	3,0
22 BH	12 00	12	* H	<i>è</i> 4	36	2.0	12	2.0	31	4 نخ	36	27	32

. 22	30	65	2.4	24	36	26	3.0	24	₹ ú	24	۲.,	25	3ι	ر ر	
12	42	2.4	116	10	50	14	50	14	50	5"	48	27	46	30	36
24	48	20	78	Žα	5.0	16	11.0	20	40	20	50	i e	5 6	10	2 2
12	52	12	ج	12	4.4	5.5	50	50	44	18	ح ہ	14	ج د	A	
, , , , , , , , , , , , , , , , , , ,	50	10	حَّة	• '			- 4		-	• `			- L		۲.,
MCLEAN	PORT	-	CTETC	148	034	180		YEAR	7						
12	48	1/1	η, п	۵ م	3.6	22	3 e	1.8	26	16	5.5	16	20	22	3.5
22	30	20	20	22	26	55	26	22	24	خخ	24	è c	24	15	26
9.0	86	-		•••	•		٠.,		•		• •	••	• •	•	76
MCLEAN	PORT	P/	CIFIC	149	(; 3 ,	180		YEAR	7						
1 4	55	20	24	20	24	٥٤	26	1 n	26	1 H	28	16	30	12	<b>3</b> 0
12	30	15	<b>1</b> 4	Ď	34	10	30	- a	32	•	3.4	-4	ű ¿	4	3 e
'n	4.0	6	36	Ą	34	6	34	A	40	6	44	4	44	4	4 2
-2	52	B	46	а	44	15	46	A	44	8	40	12	40	12	3 5
12	34	14	16	16	32	16	غ ج	16	26	16	24	16	24	14	5.4
1 A	25	20	26	۾ خ	با ج	1 P	28	٥٤	28	à n	30	ė č	30	è n	30
٥Ś	28	20	30	١١٤	2 A	-				-	<b>5</b>	••			, , ,
MCLEAN	PERT	p i	CTETC	150	Ç4.	/ P U		YEAH	1						
12	30	12	3.8	10	36	14	36	14	₹ 4	16	36	1 "	3 t.	18	26
ŽΛ	28	20	28.	Ž٥	26	جغ	Рě	18	3 4	14	36	i 4	36	10	a g
1.6	56	12	خ ۱۱	A	42	Д	44	12	a c	14	10	j 6	34	15	36
12	3,4	16	36	16	7/1	16	3.4	16	μo	16	42	1 0	36	16	3.
1.8	32	18	ŧ0	16	3 2	1.6	24	j A	26	م ج	76	i e	Se.	15	ءَ د
19	26	16	24	20	26	25	26	22	24	કર	2 /4	i a	24	1 8	۾ج
1 4	28	18	3.4	16	30	20	3.6	18	20	1 A	20	18	è١	1/1	1 a
16	18	16	<b>2</b> 0	1.4	<b>2</b> 0	10	22	10	٨ ۾	12	70	16	ي ج	16	24
16	20	1 H	26	12	24	12	22	12	ے ح	12	18	15	٤ũ	10	20
1 4	1.8	1 4	1 /4	1/4	16	14	16	14	ıĕ	14	16	1/1	14	iz	16
16	1 18	16	1.8	10	16			-		•	•	•		• •	. •
MCLEAN	Pret	F	ACTETO	151	Ç. 4 ,	/PU		YEAR	7						
1/4	20	12	22	10	22	6	22	ρ	2.0	<b>;</b> (.	24	12	26	10	20
10	18	ĮΛ	1 64	10	20	1.0	20	1.0	5.5	1.0	80	10	20	i٥	20
10	25	ξo	22	10	25	я	24	я	8.8	43	76	10	2 .	10	24
12	24	15	22	12	24	1.4	26	12	26	12	26	17	26	12	24
10	74	14	26	12	24	1.0	26	10	PA	10	30	£	26	10	26
1 0	3.0	10	Z 13	12	26	14	16	16	5.1	16	25	16	20	14	24
1.6	24	16	26	12	37	1.0	₹ ()	12	32	1 ()	30	10	34	16	₹6
1.0	34	14	₹:,	Į A	20	20	3.0	22	28	24	20	25	2e	1 0	3.5
16	3.0	1 4	₹ (j	į n	ح بر	16	3 %	20	32	20	26	ہ ج	26	(؛ خ	30
52	34	22	3.4	1 &	78	25	32					_		•	. •
MCLFAN	PTRT	v,	ACTETO	152	1.5	780		YEAR	7						
52	24	24	215	22	2.4	22	24	20	20	3.6	2 "	22	30	20	3.2
1 4	3.5	2.5	۾ <b>ر</b>	50	10	1/4	\$ P	18	30	24	3 :1	ē4	50	24	3 Ū
20	15	2/1	۲٠,	2.4	7.3	24	( ن	24	52	54	3.2	2r	ہے ج	24	م ح
24	24	21	24.	26	20	24	55	4 ج	26	20	5.5	20	24	ہ ج	24
5 0	24	16	26	1 -	2 to	18	24	50	24	18	2	14	34	12	3.2
1.4	26	18	20	1 3	74	1/4	24	12	5.5	1 4	<b>2</b> a	٩	20	6	26
1.0	24	17	22	12	<b>&gt;</b> 0	1.2	18	12	1 à	10	2/1	10	24		
MCLEAN			<b>ACTETC</b>			<b>/</b> PC		YFAF	1						
10	25	д	2.4	16	5.0	16	25	16	25	1 4	1 H	16	1 &	14	20
1 4	20	14	21,	16	26	16	20	16	<b>2</b> 0	1 4	2.0	1/4	51	1 13	20
16	18	16	1 μ	16	1 d	1.4	16	1/4	16	1 4	16	14	1 e	1/4	15
14	10	16	1.9	16	1.2	16	1 2	16	12	1 6	<b>2</b> 11	1 5	<b>2</b> (.	1 8	20
1 A	20	1 10	25	1 8	20	5.0	22	50	ڏ ۾	18	٠, ﴿	1 5	24	16	20
1.9	28	14	7.	1/4	2.2	16	ن د	l b	20						
HCI EAN	PURT		ACTETO	154		180		A F W B	1						
j A	20	14	20	16	21	Įυ	26	$T$ $\alpha$	<b>?</b> ()	14	20	15	1 હ	1/1	72
5.0	25	16	24	16	20	14	20	) A	5.5	1 P	20	16	20	16	20
1 6	25	50	25	2 n	2.2	5 0	72	50	55	1 8	20	1 12	٥.	20	25
50	25	20	27	20	2 2	50	5.5	20	214	5.0	54	1 #	24	) µ	25
Į A	<b>2</b> 0	1 P	211	1 A	71	) P	20	30	55	1 P	20	1 8	20	1 9	50

1 4	>2	1 *	21:	20	5.5	18	2:	l B	10	12	74	14	<b>3</b> 6	16	24
16	50	16	2 t	16	ž4	1 19	25	18	<i>74</i>	5"	52	5 n	76	5,	25
	PERT		71 31 C	195 23	- 05/2 26	24 - 24	26	VEAH 1	<b>ک</b> ر ا	20	2.2	1 4	2.	<b>5</b> u	25
۸۲ ۱۸	74 18	ar In	1 14	10	18	16	18	18	ی ح	16	1 ਰ	15	1 8	1 v	55
16	<b>&gt;</b> e	1.6	26	16	20			YEAR	,						
<b>U</b> = 1	Prkt		CTFIC	- 156 21	01/6 20	15	39	15	ט א	6	ج ۽	4	30	p	24
1 4	26 18	{	26 26	10	16	14	i à	14	1 14	12	21,	14	10	10	22
111	25	10	ر 2	in	24	10	211	10	ڊ د	15	22 13	12 14	20 18	12	ን። 18
14	16	14	1.8	1.4	10	1.4	16 16	16 14	10	14	16	1 "	10	1	16
14	th PCRT	- ( A 	TH. CTFTC	10	16 - (87	14 PG	16		, "	•	_				
MCLEAR	18	16	14	16	12	16	36	i P	54	16	30	) F	2e Ze	20 14	34
77	24	72	20	5.4	1,7	20	3.2	22	ን ( <i>ን</i> ይ	5 i)	30 26	22 22	26	1"	7 14
16	34	18	ችኮ ICTF 18	- 1 < 8 - 1 < 8	-3( ,⊹⊁	-22 09780	76	4 E A R		ζ,	, ,	• •			
MCLEA.	7909 SS	20	24 24	16	26	14	ڊ ج	12	26	14	26	1 7	ہ ج	12	25
/ b	54	ij.e	źż	1 4	<b>2</b> 0	16	22	50	20	2 r	يه ج ر، ج	1 F	24 21	12	20 15
10	18	1/1	4.4	12	20 95	14	22 18	14	، ج ع 1	15	18	14	12	16	20
1 11	2 () 2 ()	10	1 A	16	18	14	18	12	12	14	<b>&gt;</b> (-	į u	21	10	<b>2</b> (
1/4	50	1/4	2 ú	•				••							
GALLOWA				n 134		08VSD 10	16	YEAR	<i>ე</i> ვი	10	3 0	۴	46	10	16
l a	5.5	16	24 35	1 /4 1 /4	3 to 3 to	10	14	4.9	38	10	42	3.4	4. (.	1/4	t,ì
12	11 2 13 8	12	36	10	44	12	$a \in$	1 8	4.5	19	3.0	15	3r 2c	۱۰۱ ۲۰	4 J
10	₹ (1	10	10	l u	۲ ۾	18	<b>₹ 1</b>	2 Z	2 S	۱۰ ج	₹3 431	11 24	3.5	( )	نر 3 نبر 3
5.0	30	1 6	2	l a	25 24	የ	ن، رح	10	2.4	1 4	2 b	<b>2</b> e	2 e	) A	34
12	त्रह स्	17	2 F 3 H	) 5	₹ 6	12	40	įρ	3 ~	20	3.0	1 0	3 2	10	3 0
1 0	4.4	ı	E }-	2	وا له	2	۲.	4	5.4	2	5 2 6 ()	e e	4 c 5 c	b 1 11	112
1.4	ξ P	ρ	d q	۶ >	46	0 <b>5</b>	62	4	43 43	10	2.3	16	24	1 ^	21
54	11 4 3 A	e o	/12 ₹e	1 4	3.4	ie	12	15	3.4	16	3.4				
SAL(C)		Α		10 135	. (, 2	-03/8		AFVE	7		ج ۽	1+	3t	۸۶	ξμ
1/4	34	16	₹ 5	12	र्हेट रा	14	ις	14 12	34 30	15	10	n h	30	Ę	۾ ج
jя	30	1/4	7.; 26	10	1 /4	12	12	Ä	٠٠ ج	12	<b>1</b> .,	12	24	14	25
4	26 22	20	24	80	÷ .	62	74	t B	24	16	2.	1.4	24 2-	1 ft 2 <b>2</b>	22 30
10	5.5	16	20	16	22	14	20	£ 11	ر ج ان <b>ت</b>	12	ح ج ترج	22 21	2 r	18	14
50	4.2	(۱ نم د د	1 2 1 a	12	7	1 A 1 C	32 30	7 ^ 1 ?	2 4	, t	9.	້າ	4.0	٠,	u b
l Ja	3.4 46	12	د 7	-12	e i	- (	ń A	'n	3 (	b	2 1	12	24	14	24
1/4	2.5				,			YFAR	, ,						
GALLER				Ir 13	5 : 3 20	783 16	٦ ز	16	20	14	ż,	16	21	12	5.5
14	2 G	j e	2 a 2 a	, ,	22	ڄُ	2.5	·μ	له د	ρ	5.5	Д	24	Д	2 v
, ,	18	6	1 2	10	21	А	25	A	26	6	2 a 4 .	e P	2 ê 11 ê	Ł b	5 S
A	ي ج	i i	21:	h	3.0	2 7 5	7 <u>7</u> 7	5 16	\$ <del>2</del> 4	16	5.7	ء ۽	2.0	16	1 8
12	34 1 P	16	22 22	۱۰ ج ۱۱	25 15	۶.	ج ز		1.7	•					
GALLE			A TIE			3/FJ		AFVE				41	24	4	22
10	12	1 0	12	(1	21	4	5.		24	10	۳. د خ	12	50	_	2
А	24			10	21 20	15	57		ن خ	10	13	10		10	1 =
12	20 16	12		2	، ج	6	7 2	a a	55	5	1.6			. n	16
۲٬۱	16	- 2	51	- 9	1 14	• /l	16		14 26		بر 1 ر ۳ ر	_			
′3					12	۾ ۾	1 (		24		به م				
SALLO		ĮΛ	1 26 1111	7][ 1]	ن در		r <b>6</b>	VF A							
SALLE	441		24 7 12 7 15	• .	•										

					_				_						
۴	25	6	24	10	26	10	28	6	24	14	24	4	22	4	26
<b>A</b>	26	1.0	2 €	17	211	1/4	5 1	16	5 C	16	24	2 r	24	1 A	2.4
1 0	25	1.0	20	14	2.5	16	25	20	24	1#	22	1 8	2١	12	2
1 //	26	20	22	12	211	1.4	30	16	50	16	2.5	16	10	16	1 2
i 6	1.8	14	1 2	12	10	16	2 0	16	څڅ	14	20	14	يَ ﴿	• • •	. 5
GALLOW			LASTE	•	-			YLAR	7		r ()	1.4	, (		
_			-											_	
А	18	12	14	۲۱	1.4	12	14	12	14	10	1.4	A	16	2	24
^	24	2	<b>7</b> (	р	1.8	6	16	6	16	Д	10	ρ	56	<b>-</b> 4	4.0
<b>~</b> 30	55	. p	ر،	٠,٥	30	- (1	3.2	<del>-</del> 2	32	А	20	P	2.2	12	ی ح
12	>5	/1	1 15	4	14 4	A	26	12	3.5	14	24	16	24	12	26
ہ ج	24	22	26	1.8	25	16	20	12	2.1	1 8	25				-
GALLOR	ΛY	A 1	1L41 11	in tan	04,	/ A Q		4 F V 5	7						
a	16	ρ	14	a	16	1.0	14	н	1.4	4	14	4	5.1	6	15
A	14	12	12	1.7	1 14	16	20	A	10	ρ	1.7		٠,٠		_
10	12	6	,,	1,	P	6	6							6	Α.
_						4		<b>,</b>	10	<b>→</b> 5	21,	-6	Şυ	0	10
4	16	4	1.2	,	1 (,		ć	4	0	2	1 0	2	10	7	16
Ŋ	10	5	۱ ن	4)	1.0	C	д	n	D.	5	b	4)	t	/1	c
4	6	4	1;	74	r	4	10	b	۴.	Ц	p	(:	ť	n	8
n	换	a	14	>	1.6	2	Ę <b>3</b>	2	t	م	6	11	ť	/4	c
2	6	2	b	>	Ł	2	É	2	6	4	8	4	t	4	Д
4	6	5	t												
GALLEW	Α٧	۸ ۲	۲۱, ۸۰, ۲۱	ir jai	05	/F.)		YFAH	7						
0	10	6	21	1)	10	6	8	à	ĺβ	6	12	p	16	D	1.
4	22	10	26	>	20	Ã	18	4	6	2	8	u			16
,		4			F 67	i i			-	4			t	4	b
	10		Ŋ	'!			6	>	0		6	4		4	¢
n	H	0	щ	>	12	0	16	9	14	()	1 0	ų	۱ć	4	12
a	10	д	1 1;	4	1.4	5	12	0	2	• •	5	Ç	~	~ 2	2
- 2	5	<b>+</b> ≥	4:	د -	4	• S	Ü	+1	5	ti	2	2	u	7	14
0	4														
GALLEN	A Y	A ·	የርላ: 1	(C 1 1)		180		YEAR	7						
n	6	٠,>	14	- 2	44	2	8	5	4	2	4	r	b	-2	ą
10	16	,>	1 /	>	r	h	μ	A	10	۴	١ )	6	Ċ	4	1 8
ر	12	-4	1 2	4	1.0	я	12	ρ	1.0	'n	10	Ä	10	ĸ	12
Д	1.4	,a	1 5	j	18	Д	10	Д	10	μ	19	£	10	1 7	
F	16	ė	1.,	در	1.0	Ą	10	Д	10	H	16				12
	12			ρ	1.0	A	10					<del>ا</del> م	1.0	^	١à
F ( Muss )		•	12				1.0	, b	12	6	1 0	~	ا ۱	•	10
C( MARK			867F71	_				YEAR	7			_			
۾ ح	32	۶.	τ,,	27	u l,	l b	7 2	5.0	4.5	1 8	7 ۱۱	22	16	22	40
24	45	1 8	ر ۱،	10	9.6	16	95	ء، نے	43	24	3 U	24	3 c	۶۶	3 ≈
5.0	4/4	6.2	4.4	22	44	1.6	7 ،،	1.0	5.4	1 12	43	14	50	20	44
2 4	ξH	24	31:	11 ثم	7.1	2 p	32	ام نے	34	2.6	30	ë P	3 /2	30	3 4
3.0	4.4	10	₹6	3 7	30	CP	<b>3</b> , 8	ية نے	500	24	4.0	àb	aè	24	11.2
211	46	r ^	11 73	1.4	(د په ا	2.0	44	51,	42	24	76	è 4	3 c	۱۱ ج	30
ن ح	3.2	رخ	2 =	20	7	تع نے	3 C	4ج	5 .	24	₹6	ع ج	31.	۾ ج	36
۾ خ	311	هرخ	1	ه څ	11	3.6	30	26	34	26					
· · · · · · · · · · · · · · · · · · ·	30	r	. 0	· · ·	. ,	£ 1.	10	۲,	, ,	21	36	5 4	36	5/1	35
54															
- C( अस्टब			ACTETO			///		4644		•	_	_	_		
یم نے	15	24	ن ۲	C. F.	\$ 14	6/1	30	2,2	32	5.1	ج ۽	1 6	36	16	a C
لا نے	\$ (1	2.4	۲,۰	ا خ	4 6	1 14	4 (	1 ~	1.1	ä٠	44.4	27	44,	16	44
22	40	27	ŧμ	16	43.62	1 8	44	۱، ج	40	20	'a ç-	2.0	54	2.5	3.6
16	24	20	21.0	6.1	40	۾ ح	30	26	<i>ہ</i> ج	26	3 7	ē P	3 2	2 P	4.5
26	3.8	24	تے ا	84	4 C	30	40	30	ι,	24	42	لانے	114	211	uż
۾ ج	40	12	di.	7.1	t: 2	2.5	11.0	ح نے	4.2	ناخ	45	77	40	20	36
آم ج	40	22	30	25	3,	en.	$n_{i,j}$	﴿خ	3.4	2.2		ځځ	34	25	18
24	10	24	1,	7.5	31	و نے	1.,	ج ح	ξc	22	3 5	24			16
211	36	÷4	1	÷ 1.	ž ,	٨.	₹ 0	5.1	3,	54	3.0		36	54	
7/1	30				14	52		-				24	50	د) ج	10
		å6	16 16 11 11				a 32	24	_ ₹0	c A	3.8	54	34		
CCMARH			AC 1+ 10			*11//		AEVE	7	•					
26	15	<i>2</i> 0	4.0	2.4	14	26	3.2	5/1	54	54	34	2 P	5 1	م ح	43
<b>ه</b> ر	<b>3</b> A	24	<b>7</b> A		L fi	۾ ج	36	2.2	3.4	3 44	6.2	32	46	32	u c
30	40	29	45	٠, د	46	1.2	44	15	۲۰ ک	16	۴ (	50	6.6	511	4+

									_						
ŞΡ	40	3.2	40	32	34	32	3.5	32	3 H	35	38	3 C	4	511	5 &
20	56	24	ج ۽	مح	46	30	4.4	32	36	32	36	4 ج	lic	2 کے	1. 14
16	56	12	42	16	ج ،	20	9.11	ž 4	44	26	44	24	30	2 8	1,
30	38	26	40	à١	54	16	54	٥٩	54	16	58	20	5 ن	_	,
CUMMERC			CTFTC	134	11/		, -	_	7	•	•	-	•		
	-			-	5.0		4 7		54	20	11 4		4 -		_
24	44	2.2	48	1 8	-	15	4.5	14				16		16	50
5.0	46	م ج	44	۱۱ ج	114	22	112	4 5	40	<b>3</b> n	13	30	3 c	30	16
30	30	5.5	B (4	1 :)	۾ په	10	hu	1 4	60	14	ē 1	18	46	511	45
ں ج	<b>3.8</b>	5.5	T p	2 A	42	38	41	A C	34	2 P	3.4	24	3 v	2 H	30
۾ ج	30	۾ خ	32	a c	3.2	5 b	3.2	30	ړ≀	30	3.2	24	34	26	36
24	38	26	1.7	54	45	مح	40	36	42	30	112	36	46	3 A	40
	35	ŽΑ	1.1	£.		-	•	-	-		~	-	_	-	0
A 6		-		135		119		YEAR	7						
CLHMERC			CIFIC				• •			0	7.	20	7 .	2.0	
22	34	20	1 to	5.5	3 t	24	30	54	11 5	20	35	2 P	3 c	24	35
7.6	12	28	<b>3</b> ()	2 A	3 G	28	3.4	18	44	10	٠. ن	3 n	34	32	36
32	46	24	44	26	36	20	40	6	54	1/4	42	5.0	3.6	50	314
5.0	38	2.0	11 15	20	40	20	3.8	5.5	30	26	30	22	34	24	36
22	32	24	7,7	22	32	2 S	32	2.5	3.8	20	3 9	ہ کے	30	20	32
	34	20	وُهُ	ĺÁ	3.4	16	36	16	38	18	30	20	24	٦٥	1
۸ ک			•				7 b	16	40	1 0	112	16	54		
5 0	32	50	3.2	50	32	18	מי		•	1.	" "	10	,	12	<b>5</b> 0
CCWALH		P.	ACTFIC			/79		• • • • • • • • • • • • • • • • • • • •	7	_					
10	50	è 4	71 12	2 P	ž h	<b>3</b> N	3.5	30	32	30	3.2	3 C	36	3 0	12
3.0	32	3.0	٦,٢	3.0	3,4	2 <i>h</i>	36	30	34	3 r	15	3 C	3 <i>è</i>	5 B	35
n Ġ	3.2	3.0	32	2 H	3 4	2 A	3.4	30	34	2.8	3 ()	2.8	36	3 1	32
24	17	مج	36	رڌِ	36	20	34	20	32	2.5	3.4	۾ج	3 6	26	34
	30	26	7 ti	۾َرَ	32	ع ج	30	26	30	26	¥ (1)	26	30	26	30
26				-	3 6	١,				24			34		
26	30	74	3.5	2 1		26	3.4	8 4	3 2		12	4ع		24	<b>4</b> <i>t</i> <sub>i</sub>
22	36	2.0	₹6	50	3.6	50	ti C	50	30	20	ii ij	20	41	50	44
۸ ج	42	2 n	// i)	5 n	34	20	34	1 A	16	50	3 11	22	3,	52	3)
22	30	20	م ح	22	2 8										
CCMMERC	° F	۶	ACTETO	. 137	6.1	/F0		YFAR	7						
50	24	6.5	28	22	2 %	2.5	ت ک	2.5	46	20	25	Į n	3 G	16	30
18	32	โห	۾	ρ'n	36	20	54	25	₹.0	20	3.1	2.2	30	211	32
	34			20	3.6	۾ڄ	36	35	36	30	د 3	24	3 6	ŽΑ	32
45		26	<b>3</b> (1)						43	30	3 8	2 a	46	30	44
24	<b>\$</b> 0	30	36	32	36	32	3.8	32							
a S	44	26	n is	22	= 4	16	56	1 2	54	1 8	5.2	2 2	54	27	40
5 0	4.8	ë 0	5 ()	Į A	48	S 0	42	18	5 4	16	د ۶	22	4 e	54	46
22	48	24	/1 b	κج	116	78	114	۾ح	4.4	30	Вą	30	414	٩٢	116
211	48	20	م	Į A	60	0 کے	52	22	5.2	26	50	28	1) E	3.0	46
ăŠ	// 6	20.	44	•	_	-	_		_					-	
CCMMERI		_	ACTETO			0.81		YEAR	7						
_			-			18	4. 3	1.8	ંચલ	18	48	جح	40	20	<b>~</b> ()
βĘ	44	26	44	21	46		43	=		-		-	56	-	ري
5.0	42	5.0	(1.6	15	46	1.9	1: 2	16	48	16	46	1ê		12	
2	A 0	۴	5.5		56	6	e ()	ь	5.7	10	5.6	12	46	1 8	V, C
20	42	64	Z 15	ا، ح	36	20	42	18	110	16	ے ۔	15	54	12	40
10	48	18	11.4	22	46	26	36	54	45	24	1 t.	2.6	٩c	2 H	34
۾ج	32	6.5	12	<del>-</del>											
COMMER			ACTET	139	. / 2	2/PU		YFAR	7						
		ρĺ	41	,	'עט '	, i	0.4	10	46	ų	54	12	41	1.4	44
16	34								30	1.8	20	i A	24	į P	25
16	36	l b	10	16	34	1 8	3.0	20				_			
٥ د	26	ë 11	ט כ	50	PΗ	ں ج	76	50	برح	25	50	55	26	55	24
22	28	62	24	22	2.8	5.0	* C	25	35	55	3.2	55	32	Д	115
1.0	44	μ	44.4	Д	4.6	12	48	1.4	44	14	۶ ۶	6	46		
CIMPED	CF	ţ:	ACTET	0 14	n ca	110		YEAR	7						
52	ัวห	22	- t <sub>ij</sub>	24	26	2.2	24	ظن	28	26	7.8	26	3,	24	10
	30	611	10	ہ ج	3.2	24	12	26	30	2.4	1	مَجَ	34	ŽΑ	₹µ
22				-		54		50	46	5.5	46	50	نے نا	جج	44
24	40	26	3,4	ė b	46		116			26				ŽΑ	32
50	u S	16	46	2 1	12	24	3.0	50	34		32	5 6	3 é	_	
2 #	12	ë P	3.5	ë A	- 35	2.8	32	2 8	3.2	30	3.5	30	34	3 0	32
CUMPEB	re	þ	ACTET	C 14		5/PU		AFVB	7						
28	3.4	¿ P	32	211	30	24	2.8	24	24	24	2 A	24	26	54	26

24	26	74	26	24	۶۶	22	35	22	56	2.0	30	17	34	24	30
CLMMERC	E	FA	CTFTC	142	(+3)	180		YEAR	7			•		•	,
1 /1	45	Д	5 b	16	6.4	2.0	4 C	24	3.11	24	36	24	3 c	2.0	10
ρa	34	é A	36	2 14	14	¿P	30	45	30	24	₹ 4	55	30	وخ	₹ 8
22	42	24	36	20	36	20	12	24	32	26	ح ۲	26	3 è	24	12
δu	32	20	5.1	26	24	26	20	دا تح	<i>हे</i> 0	20	24	ž r	24	34	56
32	50	30	جَم	34	ت ج	32	ج ج	52	5 મ	36	۲.,	34	50	34	50
34	50	34	۲.0	3 A	41	36	1; B	34	5.2	34	<b>G</b> .,	30	52	34	۶ž
10	72	<i>2</i> 0	64	1 h	7.0	22	60	20	75	ž 1	7	30	50	40	ځ٠
10	48	u n	n p	40	46	42	0.4	40	// 8	30	4 /3	20	Se.	30	58
a p	30	30	52	32	41-	34	40	32	46	32	5,2	34	4+	3 A	44
COMMERC			CIÊTO	143	647			YEAR	7	<b>-</b>	- 4.	•		٠,٠	
3.0	34	34	I (i	3.0	41,	34	4 (	34	ج،،	34	4.,	36	n G	36	a g
36	40	44	۵,	12	ج ۽	40	۴č	40	44	40	116	42	u u	411	42
40	112	40	41 2	<u>.</u> 4	112	žρ	4 G	34	44	3/1	46	211	58	30	34
3.0	34	3.0	٦.,	32	3.4	3.2	34	32	3.4	3 2	34	2 P	36	,3'' A G	
4.6	34	الانع	10	e p	3.4	26	3,	ءَ ہُ	36	26	3 /4	211	n,	52	36
24	40	جخ	44	22	0.4	50	<i>L</i> 2	54	84	25	چە	۾ج	46	ŽÁ	40
24	40	ĉe	26	26	3 14	5.4	3.1	A G	38	30	47			-	40
54	30	56	<b>7</b> P	26	16	26	36	32	4 (·	30		28	4 c	24	36
-	36	24		22	ن 4	26	40		40		3 6 3 0	28	34	56	g p
PA CCMHERC	-		42 101130	144			٠. ن	4F 9 E 5 P	7	5 %	3.8	2 P	3 c	30	36
() ( ) FR()	. t . a.B.	36		34	ر د ن	40	414	אנייא		, 2					
		32	11.2		46	34		-	46	372	46	32	46	3/1	44
3 n	46	34	и e	34	5 2	34	44	34	4 %	3 4	49	40	44	34	។។
C(MHERI			114	- 22 - 145		/ P ()		W1 40							
•	-		CIFIC		i i ji De			AF VE	7			- 0			
3.4	44	24 20	ح 4	16		1.6	116	24	46	1 2	ح ہ	50	44	50	44
22	64	20	42	ā 1	42	50	3.5	5,5	3.6	50	4.7	5.0	46	16	٠ 0
16	110	14	C 1;	l u	45	16	4.2	24	40	ē4	<u>.</u> in	56	34	۾ڄ	30
PЯ	31.	۾ ج	3.5	2 11	3.0	26	3.4	26	\$ 4	20	34	25	3 e	24	38
٦٤	32	r n	s (,	2 9	3.4	24	3.4	26	38	24	40	2 t	3 c	٤٤	3.6
2 %	30	30	37.	3.0	3 4	2.5	32	26	30	3.0	49	24	44	50	46
ر ہ	46	26	46	22	ښور <i>ا</i> د -	26	36	26	31	26	3 a	24	34	26	30
4,4	36	2 13	34	ĉ۳	3 %	26	3.4	2 A	$a_{\mathcal{Q}}$	۴ ح	ج۶	۾ ج	36	50	3 e
20	38	5 ()	रव	2 11	3.5	۾ نے	36	30	3.2	54	ž ()	24	3 L	50	32
۸۶	3.2	62	26	21	2 8	26	3 (	54	56						
CLWEED	E		CIFIC			NA C		YEAR	7						
24	<b>4</b> ()	26	9,5	26	21	26	3.5	54	30	24	3.6	28	36	30	32
۾ ح	34	2 F	22	ê H	24	26	2.3	24	26	24	26	۶۶	24	20	26
1.7	ጄ (፣	1.0	₹4	12	16	14	3 2	16	26	1 8	78	1 5	3 u	18	26
1 8	28	ان نج	<b>T</b> (,	20	٠, ٢	2.2	26	24	30	26	24	26	71	26	26
24	ŽΗ	24	20	45	<i>2</i>	<i>è</i> 6	ج دے	26	2.5	¿ t.	ہ ح	26	ے دم	24	26
26	28	1.3	3 (1	ا ج	7.0	2 <b>2</b>	26	5.5	20	25	26	25	26	22	30
3 ^	34	30	קד	32	44	۾ ج	4 C	28	42	2 8	4 %	30	"e	۾ ج	36
30	ŢА	30	ι,											**	
CIMPEUL	^E	P.	CIFIC	117	ub.	/ R ()		YEAR	1						
3 0	15	50	12	30	14	30	3.2	30	32	3 O	3.4	36	34	30	34
3.0	3/4	30	3.4	äя	34	28	2 ن	30	3.8	32	45	34	46	36	3.8
3/1	3.6	3.4	<b>1</b> p	41	24	34	46	34	š e	2.6	3 0	26	3 c	a خ	30
۾ ڊ	30	ž a	ج۶	50	3%	30	32	26	36	36	35	è u	3 6	28	32
رخ	24	22	2'1	24	20	2.6	24	24	že	20	3 0		- •	•	,,
CCMMERC			161110	-		/FU	-	YEAR		<b>.</b> .					
211	26	24	213	2 1	2 -	36	28	511	<b>,</b> 2 e	22	70	24	2 t	22	26
22	26	ž 1	26	54	71	2.5	24	25	2.1	2.6	, 0	£ .,		66	70
CCHNENI			1010		_	/ P (	, ,	YEAR							
1 9	22	16	22	ן פו	22	Žμ	50	7 C # 11	<b>'3</b> (:	26	<b>9</b> 2	÷ 11	3.	2.0	3.4
۾ ڊ	28	ž ii	26	24	21.	55	24	20		50	28	24	36	54	24
CCMMEB CCMMEB		_	/ D A C T F T C			/80 /80	e 1		24	6"	5.5				
- (.C	   32	''۾ ح	4/1 4/1	۱۵۱ عر	12 /	28	<b>3</b> .9	4678		9.5	7	- 0	7	50	
2 A	50	30			12	30		45	3 0	2 P	3 ()	2 P	30	24	30
			۲,	30			32	30	32	30	3.2	32	30	3"	3.6
5 11	10	5 11	1 h	5 %	36	54	36	34	<b>3</b> /3	32	n (	32	44	3 0	/I u

<u>5</u> ^	40	2 P	49	۾ج	6.6	28	40	2 A	46	24	38	2 8	3 e	~ 0	
ه ج	36	éb	46	24	1.,	56	74	24	32	۳5	34	2 P	34	βA	40
30	32	30	iž	30	32	C 17	•	£ "	, 2	E	7.4	<b>~</b> "	34	30	30
CCHAFRO		_	כודונ	151		/ P U		YEAR	7						
30	ें दट	 ' ج	31	34	36	32	34	34	36	3.0	36	32	36		_
5.v	45	ان	'nέ	22	4.0	45	38	2 H	3 G 3 D	5.b 3	36 36			30	T M
2 B	35	ξp	1 J	31	3,2	26	. 2 C . 5 C	7.5	-		-	32	3 e	2 A	3.4
سرج	32	30		-	15				32	21,	30	ع ج	34	58	36
CUMMERC			- t2 - c - c - c	2A		78 J	3.6	26 36	45	54	38	30	44		
30			CIFIC	152	96	, 5 ú	44	YEAR	7	2.4					
EXCHANG	42	55	−≅⊅ CTF†C	12			64	54	36	54	3 u				
5 X C P A * 3 C	ነየ ፋሎ			1/48	*c	179	11.0		7	0			_		
		52 88	*8	52	E a	30	4 C	2A	40	58	# U	3 C	3e	30	34
30	36		40	3.3		30	40	ĄŞ	40	Si	40	5 %	" (	2 A	3 12
קג	38	٤٤	4.1	3 1)	3 1-	30	3.5	3 n	3 a	32	4.0	35	4 (	3>	n o
30	4.5	3.7	46	3 2	<b>T</b> ji	35	40	34	112	31	46	32	36	55	i, p
3.6	44	22	5 (j	2 A	110	50	11 15	20	5.5	55	45	16	μē	1/4	ړ ۲
20	14	16	4 4	1 4	7,4	24	/ C	56	30	32	38	34	3+	3"	3.7
32	38	4.5	ام 🖈	32	<u> </u>	32	3.0	3 ()	3 e	32	4 5	3 8	14 c	34	40
40	a 5	30	1.4	17	44	3.8	46	34	52	34	ر ۽	32	46	34	44
3.6	44	3 11	بالمؤ	32	12.6	34	46	3.4	4.8	3+	45	32	46	54	tt 😘
54	54	24	54	2 ^	ς,	26	در به	32	الم 1	31,	u H	34	44	36	4 G
36	4.0	3.6	44)	3 વ	44	36	42	32	44	32	a 4				
EXCHANG			CIFIC	147		/79		YEAR	7						
3.2	16	30	4.5	èα	۾ ۾	5 8	46	3.0	ય ટ	3.0	#4	34	ti ti	34	44
36	42	36	45	36	4.	36	<i>u</i> 2	35	شم ()	2 8	<b>~</b> 1	26	54	32	46
3/1	44	34	11 2	36	46	36	4.3	36	43	36	<i>u &gt;</i>	36	4 0	34	<i>n</i> ;
36	46	36	7 12	3,0	4.0	3 P	40	34	45	34	75	36	46	3/1	11 2
34	45	3 6	9.2	5 A	64	38	4 6	3/4	13 4	ž a	41.17	3.2	3 e	36	45
3/1	46	ξÞ	/: Z	34	7 h	36	46	511	44	34	n 5	30	34		
EXCHARG			ነር ተነ ፲ሴ	150		179		AEVB	7						
32	44	3.5	44	45	" (	26	48	5 b	40	S.a	41 (;	ع د	40	30	1.4
ه د	71.5	è A	4.5	2.6	4.5	2 b	4.3	28	45	26	4 (:	24	45	25	n p
2 ሰ	56	16	c 13	27	٤ ١١	18	56	t P	50	9 5-	5.4	1 0	56	۱۱ نے	40
5 v	45	l a	f fi	16	<b>E</b> 34	16	۴۲	14	43	14	60	18	54	۶۶	E /4
٦٨	52	į 4	" 13	50	4 64	24	4.2	Şβ	5.4	3 C	ہے ت	45	110	24	46
5 0	5 ()	ĺĦ	" to	24	۶ ۶	2 p	4 ć	30	40	34	76	5.0	40	1 14	5.8
50	<b>S</b> 1)	20	40	32	42	34	3 €	30	37	3 C	$\mu_{\rm G}$	28	40	30	40
32	4.0	3 11	40	36	٠(,	36	40	36	4.4	36	$u_{i_*}$				
EXCHAIL	· †	F	CTETC	121	C1	NB G		YFAR	7						
4 12	ate	36	45	34	E 17	36	47 C	36	جء	36	4.2	32	50	34	44
ţa	116	i u	46	34	a P	34	4 13	36	= $0$	34	κ.,	36	50	36	44
34	4 15	3.4	11.4	q n	o H	4.0	66	3,4	4 4	3 A	42	3 62	44	36	114
34	a F	34	40	ž M	11	36	4.8	36	.134	30	E ,	e P	56	30	ع ۽
32	52	3.5	10.5	30	47	34	48,	32	46	34	11 %	34	112	3/1	دې
34	14.80	36	0.7	4 2	** **	36	41.4	3+	46	34	t: o	- P	de	40	0 E
34	48	3.8	P 14	36	100	34	44	34	+ ĉ.	34	36	34	3 c	3 H	Αij
3.6	44	R.F.	22	40	02							•		-	
EXCHANG	٠,٢	¥ ÷	STETC	152	0.1	186		YEAR	1						
40	112	ų n	42	5 B	15 2	34	4.2	3 n	4.1	34	n a	36	40	40	h F
<i>a</i> >	44	3.8	44	1.0	40	36	43	36	44	32	42	3 11	u ų	34	62
3 0	2.0	A F	$n_{ij}$	3 0	95	3 P	45	42	4.	3 to	40	36	ďΰ	36	" (
3.71	34	32	ec,	30	21	2.6	1.2	24	ii b	96	4.,	3.0	46	30	4 H
<b>5</b> ^	4.4	3.0	11.2	24	·à	ء نے	u L	32	0.	30	6.4	ÃΑ	44	ĄĄ	# fi
۶́۶	42	۾ج	4.	32	4.6	-	-	•		-		-	-	(-	
EXCHANG			101210			120		YEAR	7						
30	44	و ۾	4.0	ã h	54	ė 11	6.6	24	E 4.	e P	<i>t</i> ,	é P	54	ن خ	ږ»
24	46	2.3	46	22	46	2.2	116	95	50	مخ	// H	، ع ، اخ	څڅ	211	46
5.0	څ٠	2.0	د ع	۾ج	57	30	45	ŽΆ	48	54	43	ž A	4 c	54	46
5,0	50	وَجَ	11.0	2 h	46	۾ج	42	34	36	٩٤	44	30	40	32	34
35	16	1,2	36	57	ę.	511	36	32	34	32	34	32	40	3 E 3 A	40
36	3 24	3,2	16	36	12 3.	4 A	1, 5	30	46	ž F	46	3 €	٦,	J"	
110	, , ,	. •	- 17	.1		-		3 11	٠.	£ '	., 6.				

EXCHAP	C.F	F	ACTETO	15.	4 62	/8u		YEAR	7						
3.0	 56	36	K ()	34	48	32	48	36	بر ں '	36	44	36	u e	31	
32	50	32	۾ ۽	32	5 (1	34	F (	32	52	3.1 3.11	5 2	Ž A	56	۾ ۾ خ	4.F K.b
nُر	٩6	2 #	ج.	2n	54	30	50	30	46	j. ∂P	٠. ج ج	žμ	5e	34	
3.0	40	3+	114	3/1	44	3 2	1,6	34	42	36	41,	36	4 (	-	// C
20	62	34	45	32	46	36	40	34	1,2	35	42	34	40	36	112
THAPF		-	ACTETO			/79		YEAR	7	7.6	٠. ٢	7.4	0	3.8	42
102	116	96	116	9 8	100	56	116	96	108	95	105	96	10.	9.8	403
9/1	110	5 n	112	46	116	84	120	35	112	44		90	102		105
90	120	ç e	111	92	112	94	114	ځه	118		123		116	92	116
4.6	110	ÇД	100	Çñ	106	94	110	90	-	91	117	97	122	95	111
9,0	100	94	106	92	114	e P	155		110	9.2	110	911	105	94	106
92	110	94	-	57	109	99		82	122	74	1 7 2	£ 2	142	£ 6	124
20	99	93	110		9.9	96	1 ^ 7	99	197	98	104	99	103	GA	100
		-	-	9 1		36		96	9 19	d h	100	G FI	100	9.8	100
97	101	97	101	4 %	100		100	9,8	100	160	172	97	103	94	104
96	110	G A	100	97	C.71	97	99	97	99	97	99	<b>47</b>	94	43	95
70.40=	04	۶۶ _	94	92		90	C 4	90	94	8.0	93				
TRADE	• •		ACTETC			/79		YEAR			_				
9.0	60	94	66	92	Ç u	9.0	96	ЯĠ	و ي	υ <del>(</del> -	9.6	67	1 0 1	۶ ۶	116
8.2	110	9.6	100	86	107	F 6	ďδ	30	В'n	90	c 6	b by	96	90	9 0
FQ	9	8.0	101	Pα	105	91	101	31	101	3.0	100	91	101	91	101
9,2	105	92	105	92	T u Č	9.2	100	91	<b>G Q</b>	91	69	<b>G</b> (	100	Ω /‡	104
97	104	29	103	13.15	103	86	105	a ú	100	94	98	94	96	65	94
QC	101	9.6	100	C 1	100	94	100	97	102	99	105	42	100	98	104
d Y	104	102	106	14,7	1 C #:	g p	164	9.8	104	94	114	96	10%	96	108
94	100	G F	104	C.V	100	95	105	94	100	9:,	714	92	116	92	106
9.0	108	C 11	104	92	100	49	111	A A	110	٤٦	120	20	120	8.3	117
72	130	14	133	7 /1	130	7.8	12:	H <b>2</b>	115	PF	114	92	112		
THADE			31 31 D \$			179		YEAR	7						
9/1	110	9.5	100	9 6	104	97	105	96	103	PA	112	9.2	114	96	110
9,9	104	99	105	146	105	7,9	105	9.8	113	9.2	110	9.4	110	9/4	118
92	120	95	115	96	118	96	120	3.8	114	100	114	GF	114	Q A	116
0 9	114	100	112	34	16.9	34	104	9.6	102	सु	G M	26	100	1.6	105
ם א	OH	€ 6	100	56	100	€.6	102	MA	مه ی	۲ خ	9 j.	9.6	9 6	G (1	9 8
0.4	104	94	Cβ	9.2	1.5	16	104	9/1	108	93	Ģς	97	107	97	107
G A	108	ς ς	107	G 4	100	96	104	95	103	GA	102	G H	100	45	104
100	104	49	103	37	1.0.1	96	100								
TRACE			ACTETO	. 15		/79		YEAR	7						
92	9.0	91	0.0	94	C. Fr	91	CE	Ήď	95	91	93	56	94	9.0	94
PФ	95	<i>)-</i> A	c c	ת יק	C ·1	۾ ۾	0.6	PΡ	34	p $p$	c c	HΘ	٩٤	Łρ	90
AA	9.9	6.3	100	63	101	7 P	168	/ P	1(6	74	11:	67	100	# 2	102
2 A	OA	ħΝ	1000	e 6	٠.	26	100	46	100	8.6	100	86	108	FA	102
HA	104	μp	100	FF	45	i, h	9.6	16.0	97	مکر تم	100	11.3	99	A A	100
an	101	96	106	٤٥	1 ( 1	9.0	102	įΑ	162	9.7	101	0.0	ۍ و	9/1	9 52
O (I	102	54	104	9:1	1 € e	96	100	G P	164	96	165	GF	190	94	160
A P	105														
TRADE		٤	ACTETO	15	9 12	179		YEAR	7						
94	106	51	111	92	1 1 1.	<sub>21</sub> G	105	91	121	<i>i</i> :7	125	PF	120	FA	120
9.0	118	<b>e 3</b>	121	66	128	e 4	120	Fü	178	P 4	120	6.2	100	ي د	145
74	128	76	176	40	112	87	115	<b>41</b>	195	r, H	114	ci 1	117	74	120
75	123	7.4	124	16	172	78	118	74	124	7.4	138	76	130	7 A	120
A /I	114	6 v	116	A g	116	12 7	118	μд	114	54	108	9.4	104	, <b>c</b>	105
7.0	113	93	111	92	112	90	110	H 7	130	9.2	122	72	150	1.2	120
8/1	120	Pρ	110	F 7	113	8.2	121	76	174	ج آر	122	66	116	9.5	108
9 2	104	Çβ	104	A 11	110	92	114	94	112	g Ē.	111			,	•
THAME		F	ACTETO			180	-	YEAR	, -						
40	114	91	113	3/1	116	96	104	9.0	193	100	104	160	104	100	104
Qp	106	G A	106	3.8	106	100	106	100	104	G.P	104	1 ( 1)	104	101	103
99	105	G P	104	3.8	104	G P	102	94	9.5	ch	104	H 4	100	FU	4.2
93	103	911	10.4	G A	104	37	103	96	100	66	102	c 7	161	97	101
97	105	94	100	45	97	94	9.6	$\mu$	g e	9.2	نون			•	

TRAPE		¢	ACTETO	161	617	/ P ()		YEAR	7						
,i a	105	c 6	104	1. et	106	۶ ۶	112	6.0	112	8.1	107	7 F	116	77	113
7 //	114	16	114	7 14	112	78	114	16	114	76	112	è4	114	F-11	11
+4	110	£ħ	104		_										
THADE			AC TETC	14,		/ PO	_	AFVB	7						
<b>^</b>	24	ti o	26	1	24	. 6	* 0	4	20	r t	58	6	24	a	2 5
1 0	26	μ	21	4	70	10	1.8	10	14	16	24	1 5	26	1 4	22
<i>1</i> B	25	12	الم ج	16	25	16	2 è	15	24	20	2 A	<i>j.</i> (.	21	1 =	2.5
16	ن <b>ح</b>	18	20	15	20	18	7.4	16	24	16	20	1.0	ے تے	1 1	ح ح
12	24	17	24	17	2 4	12	23	12	24	12	2.5	12	26	12	<b>&gt;</b> (
12	20	12	2 (,	12	1 "	12	10	12	20	12	2.0	1 0	2.	10	<b>≥</b> c
10	20	10	20	10	2 à	10	20	15	1 4	15	18	Ą	26	4	24
6	2 <i>2</i> 50	12	2 (j	1.3	24 36	15	22	10	24	10	2 A	£	26	ц	£ 13
-4 ^	44	-4	د ع د ۱،	4 - 4	2.65 2.86	0.4	3 ¢	, >	38	. ?	40	4	40	0	46
	24	- 4	۲ -	- '1	4	'4	15	15	30	15	3 u	16	5 c	15	26
TRACE	~ ~	r:	ACT; [C	16	2 62	/ A (		YEAR	77						
18	5.0	าห์	26	16	êë	16	<b>2</b> 0	16	7 2 მ	1.6	1 0	1.6	1		
16	درج	1 0	25	16	25	14	24	-		16	18	16	1 e	16	18
18	26	1 6	24	1 14	ξű	16	59	6	24	10	20	36	"(	3.6	20
~ <i>,</i>	36	Ä		n	20		25	16	34	12	76	1 c	26	1/1	16
	1 14		24 21	A	ē 4	10		10	18	12	1 5	17	16	12	16
10	24	b V		я	25	Į.	26 24	ų	24	<b>(</b>	26	<b>A</b>	2 t	4	24
	16		2 č		44	'n	ζ4 3 ρ	6	2.1	(1	29	()	34	- 4	4.0
- 2	30	= 4 #	45	- 4	3.2			<del>=</del> (4	36	u	36	4	7.4	а	26
taver zavet	*1)		I, ACTETC	12		10 -03/8	30	VCAD	•						
4 / 1/17	ن ج	P.	24	1 m.	65	-113 <b>γ</b> C		YEAR	1	4.5	٠.				
	16	10	2.	 ج بـ	35	<b>≈</b> 6	24	12	25	12	24	1?	2 c	10	20
1 0	26				20		40		5.4		74	, P	24	10	24
12	۲ <u>۰</u>	12	ر ر در د	15		16	18	14	50	12	20	12	۵۲	10	24
12		171	۲,	! ^	25	15	23	15	26	14	5.5	14	50	15	20
12	<b>ب</b> ر ج	۳ ۲۶	٦,		4 A	- 6	32	10	24	16	<i>د</i> <b>ر</b>	15	25	1 4	30
12	36 24	τ>	14 cg	12 - a	3.6	12	3.2	14	32	15	3 6	16	26	16	56
! // A	a.	12	7	ب. د ا	2 d	14	42 24	10	3.6	12	3 0	10	30	ļi D	36
	3.6	, c	<b>1</b> )	10	نہ ج	16	24	14	26	15	2 p	12	2 t	P	14
16	26	_	• 3	1 ''	•	1.6	74	16	24	16	2 ·	14	76	14	24
THARF	70	0	ACTETO	1 m	e	/PJ		YEAH	,						
14	24	16	#6.716 24	4.5	` 2 e	16	24	18	ں ج	1 0	٠.	- 0	٠,		*
12	32	15	رَة	12	2 4	10	34	م ا خ ا	ں م تر ۲	4	<b>2</b> )	ē0	25	1 4	30
10	7 E	1 8	25	10	1 4	Α,	12	_		12	44	10	3.6	16	26
12	14	15	14	12	14	ج)	14	1 O 1 O	1 4		1 n	12	14	1 ^	14
10	1 2	10	۱،۰ د ۱	10	12	Į P	20	16	20	1 () 1 ()	€ 1) 4 .a	15	1 6	12	14
16	) (·	( P	2 2	4)	7 E	4,	7 (	10	· · ·	) <b>4</b>	1 +	16	3 6	15	50
THACE	71.		ACTETO			100		YFAR	7						
16	٦٢	1 ຄົ	ع ۱ ۱ ۱ س ۱۰ ح	-	22	20	72	10	24	16	24	15	<b>3.</b>		
12	26	12	ź.	12	21	15	24	12	24	12	21	16	77 22	14	16
(2	24	Ĭ n	۶,۰	12	£ 6	19	26	H	21	16		) C		•	
1.0	5.	12	30	ı A	32	וין	9 ji	Â	26	e A	25	12	2 H	<b>б</b>	70
,	\$ 15	រ៍	₹6.	ų	4 5	10	38	14	34	P	5.4 3.6	) C (4	34		36
4	24	д	٠,٢	12	¥ (:	10	24	10	24	Ą	20	6	25 14	A	26 24
12	20	12	۱ ج	12	ن ج	• •	Ç ·•	1 ()	, ,	•	80	c	; "		64
TUAGE	~ 0		ACTETC			/ R il		VEAR	,						
10	28	10	#Ç\F\1. ₹ე	12	31	15	20	10	24	; e	20	ı A	24		27
12	24	12	ن ج	12	ج ج	17	3 g	-2	46	<b>4</b> €	48	- A	144	14	0.5
2	34	ځ	4.5	17	44	5	₹ (	- 6	ج ج ح ج	P P	6 6 6 5	4		10	9 H
-/1	40	* h	e a	• ft	44	e P	u ç	r a	10	a a	( ) 3 a	10			7 / C
10	26	12	36	0	46	6	3 e	4	15	12	7.0 7.4	10	3 e 3 è	12	i,
16	28	16	24	12	ąρ	ū	26	••	٠, د	16	7.4	1	76	1 -	٠.
THACE	<i>e</i> 0		ACTETC	-		180		YEAR	7						
16	24	16	79	16	26	10	3.6	7 C H 7	16	ħ	* 6	۶	3 h	,	46
-/1	48	0	46	• 2	11 6	٦	1.0	ê	4 L	ü	42	1.	3n 34	16	20
- 11		V	. 0			•	.,	•	• •	•	** *	1.	۶,	10	, ,

	7.4		٥.		2.5	16	ρc	3 A	22	16	18	1 /1	10	14	16
) 6	フィ	16	2 h	1 9	20	16	20	12	1 12	1.0	àz	12	7,	10	25
1 1	20	12	2 d	12	۶,۰	u	26	6	3 0	1.0	2 .	17	21	16	2,
10	22	18	2:	1,7	24	1.8	2 ;	20	24	2 (1	ē .	à c	26	20	24
1 ^	24	ج ج	2.4	22	211	ر م	23	50	22	اج ج	2.,	1 H	24	16	51
م ج	34	10	3 /	۱۶	1,	Ē	3.4	12	12	ح 1	a z	10	3 c	10	34
1 4 A	14	10	زه	10	3.0	18	32	16	20	80	25	20	24	į A	22
1 0	20	16	ح ٔ ج	•		-	-	•	_			_			_
FIMALE			ည်းနောင်	136		79		YEAR	7						
7.8	ម ()	77	arç	7.0	pi (	79	۶ 1	79	Pi	75	F 3	78	Αц	76	۲ ۲
7.7	F1	7 A		16	4 -	7.8	ΕĊ	15	۶5	7 //	د ع	7.0	٥, د	64	c P
F /1	9	+4	100	0.1	1 x 24	04	192	7.0	35	72	9 Z	66	100	54	123
51	103	'5 A	1 . 2	5 H	1 ~ 6	7 c	ກຸລ	b n	9.5	7.0	ح ۹	7 n	44	7.	96
1.2	100	c 3	23	n 7	101	e 7	ې ت	7 F	9.5	76	$\mathbf{c}_{i,j}$	7 <del>/-</del>	90	77	P 7
17	я 7	77	nγ	7.0	£ 63	7 17	Pι	7 A	E O	7.8	ρų	17	4 3	7 P	PA
7.7	3.1	7 G	# 1	79	2 1	79	٠:	711	5 9	75	2 ۾	77	F 3	<b>ج</b> ۾	£ /4
4.2	<b>Q</b> (4)	۾ ۾	A /,	·- 7	# Q	2.0	P /.	ر ع	P II	£ ≥	F 1	r, Ž	A 4	R S	F 7
FIDANCE			A C * F 1 1.	1.55				YEAR	1	• .			•		
14	ج ن	73	ر" الو	7 4	я () 	7 4	» ;	75	٤ ع	7.6	ρ.,	16	7 t	77	79
7.7	, Q	17	7.;	; 5	77	75	77	74	7.4	70	7 .	71	75 77	72	7 u
12	7 17	12	7 m	7 -4	۴,	7.2	£ (;	71	7 /	72	7 A	71	// A.J	71 74	<sup>6</sup> 1
7 4	.1	7.2	<b>7</b> 6	7.3	7 e	72	7.7	70	7 11	74	9 y 75	77 72	7 c	73	7 6 7 5
7/4	76	/3	75	; ;	75 80	73 c a	75	7 3	75 65	73 65	P 3	65	A 5	65	P 5
7 1	79	7 (:	n n	7 :	79	69	6 č 7 7	7 N	ПЭ Яц	73	75	72	76	7 1	77
Ļ 0	ح ۾	7 ()	я <sub>ц</sub>	4.3	ر . ب	7 6	<i>+</i> 6	7 ti	ر د	76	P /5	75	μį	75	67
71	75	74	F 14	77 12	9.	20	0.0	7.6 7.8	84	7.0	, ,,	1.5		, ,	` '
77	6.7		9.7 ACTA TO			/74	٠٠ (.	AF VP	7						
\$ 1 " 4 × C1	r ກິດ	7.4	71 at D 5	72	, בי היי	26	٨٠	72	ંગન	6.6	ر 🕻	7.7	ρ۶	72	e e
7 4	46	14	4	16	F	76	۶.	7.1	A II	10	وأع	7 P	30	7 P	કંક
7.4	16	7 1		26	F h	72	ء ء	21.4	G ij	02	10.4	έC	9,5	62	ج ۽
76	C	7.0	? .	; à	100	ι: 0	16.9	63	0.0	و, دا	ς,	1,0	9,	70	c ii
1.6	r. n.	, ,	ं <b>ह</b> १८१	7.7	ે કે પ્ર	7.0	12	7 H	ح ء	7.0	દુંત	75	٠,٠	76	P 14
7 /1	13.60	16	<b>c</b> .,	71	ηÇ	7.0	ج ہ	7.4	Gig	7 n	ς ,	16	S. P.	76	αų
7.6	91	10	ر :>	7	c۶	17	ρĞ	7 h	Ph	7 5	د ه	14	μU	72	P.5
7.3	74	7 3	7 ,	7.3	17	14	7.3								
FILLANC		-	ACTE 10		1 12	179	-	4678	7						
16	7 H	2.4	7	12	εţ	7 '3	ې م	76	ن ج	7.5	ج ۶	17	ے م	77	F-1
7.7	я <b> į</b>	F 0	۶ :	<sub>e l</sub> a	p. i.	o P	۶.,	6.3	л.,	íè	р	7.1	ΑJ	7 '	ВC
7.0	fe 1 *	100	0,3	10	₽ C	7.4	7 0	70	7 3	55	نے ع	5 4	ЯÞ	ه ره	C 14
5.6	$a_{ij}$	( 4	الإه	٠, ٢,	91	60	\$1 i	19.0	<b>1</b>	6.4	P 8	r 4	۽ د	60	Fe
-0	نام	13 P	27	$t = i \frac{1}{4}$	pr +-	15.8	ي ہو	56	એ ું	56	G . i				
FILLER	•	ř	7550 %	1 1		/19		7 F A G	7				_		
5,2	ح :۲	5.6	Ċ:	:	ته ع	e 4	ړل عو	e 4	а, ғ	5.0	4 ک	26	81	r (1	ΑU
,. p	1 c	<b>4</b> 4	4 1	2.5	P 2	د ک	£ 5	ch	F 2	اح ۲۰	د ع	5.5	44	۲,۶	9 (
ب ج	30	F 3	G.Z		e p	6.5	0.5	6.0	8.0	• 14	A K	5 H	μ,.	6.5	۲,
7 ^	αι		فو دو	P 1	PA	15 N	FZ	7.0	7 -	7.0	74	68	ي <u>د</u> د	60	# 1
- ج	~ 1	10	<sub>ا</sub> بر	12	F. 13	17	φ.,	7.4	я <sub>.</sub>	H 2	۴4	72	94	73	A 3
7.6	G-1	7 1	3.5	7.0	84	6.5	8.8		_						
FIMALC			: ACT1 10		9 (1			AEYE					4.0		٥.
F A	0.11	c P	C 13	•	154	60	110	ę n	100	61	10:	r, e	100	64	9.6
FF	ح د.	12	9.7	1 1	F .	15	F.	1 h	ء د	7 6	F p	76	F.E.	7 P	9.9
74	P 6	7.7	n <i>j</i>	7 /-	نز د	16	6 d	7.9	30	, ~	104	6.5	1 '' c	72	5.2
<i>i 1</i> 1	0.4	72	g.,	17	G (1	6.7	104	54	100	5 *	1(2	20	1 1 e	54	به مح د کان
5.6	100	6.2	G .;	<i>i</i> :	9 6	g (I	6.7	6 <sup>si</sup>	5.5	12	G 11	7 4	46	72	<b>ب</b> ع ح
612.4	94	6.6	G,	, 1-	56	<u>.</u>		we a s	,						
£ 1 2 4 4 C			246 11 11	(, ) ;		-0671 38	٠, ۲,	4614 37	ج ۲	32	ج ۽	36	4 6	36	46
34	∕ <sub>a</sub> H . •	3.7	ς,	,	# P	26 20	٠. د ز	20 20	45	ع د ك لا	ج ۽	54	ت. در.	54	5 2
5 A	96	\$ '\ \$ '\	د <sub>()</sub> د	• ,	- 6	2.4 2.4	F. (	E A	٠ <u>٠</u>	<u>۲</u> ۲		٠.	٤,	24	٠,
3.0	66		۲.	20	6	1 6		ť	E .,	le	ج ۽	١١۾	50	ہ ج	ν
٠,٠	0.75	£ 1	• .	<i>c</i>	r	4 7	•	·	• • •	10	۲.	۲.	, ,		

211	5 ک	2.0	1. F	٧.	c µ	3 ()	r,	5/4	4.6	36	6.3	5.	" c	36	u ()
3 :	44	3.6	Z1 👍		116	3+		_		_				-	
_				5 h			44	5 ~		30	9.	5 %	44	• (1	44
40	44	3 12	71.5	4 1	e (	44	€ ^	5 14	ہ۔ ی	( -	ر ء	34	7 (	32	A 4
<b>4</b> :	58	14	6 10	30	1. 6.	34	C +.	3 6	Ε.	\$ e-	۲,.	4.5	50	3 a	5.4
3.0	9.5	3.2	F :	ر ز	نړ په	54	۲,	<b>3</b> (4	r, <sub>E</sub>	-	٠,			_	
		-		-				•	., c	3 *	- (	.5 4	ح ز	3 12	/i <del>_</del>
40	44	44 (	t) 1	4 )	14.14	40	7) 🙀	4.0	4.4	1, 1	4.5	14 F	14 14	40	44
40	40	3.0	L	32	1	3.2	<b>r</b> , ,:	30	e	5 1	د ج	5 =	50	32	ږ۶
		-						-		-				-	-
3 9	50	34	۲,	\$ 13	C :	46	د ر	42	, ~	42	43	تم ب	51	45	S ()
4.2	5 (	رے د.	•	4.3	ι,	12.23	40 /								
FINALCE		ş* •	17. 18. 18	. 1.1	100	/ B .*		YEAR	,						
							_								
₹ 6	32 C	3 )	*, *	3 1	46	·* ()	. 7	14 15	(12)	e 1	ہے ،	40	Li 14	45	12.44
112	10	44.4	5.2	٠, ^	1, ,,	24	1000	4.0	11:	40	0.3	ų ∩	110	., n	44
3.4	4.15	ţ;		ţ p.	,	34.		35		3 0					
		-	· c				١. پ		* *	-	<i>ii</i> .	3/	۾ لا	ځ <b>د</b>	и (,
34	40	3 4	1	3 h		3.6	نم دا	3 1	11.4	32	11 5	Ìυ	44 to	76	11.34
4 نے	40	م ح	۲.	2.5	۲,	2 +	قر د د	25		26	ے ،،	28	44	211	.1.4
		برج.			٤,			-						-	.16
۴ نے	uh	6.5	6.5	ž a	- 1	ê a	10	25	ς,	55	ج ۽	c 4	الم الح	21.	< 1j
ر، نے	تر ور														
FINAKOF		6.5	(111)	1 46	i	180		YEAR	7						
					ς,:						_				
26	المراحة	è 4	5 2	21	•	2 8	F .;	2 5	٠٠ در	21.	٠,	د رح	5 6	32	48
₹ /1	4 14	5.4	1. 6	7 1.		34	-1.4	36	0.3	3 4	₹ ∂	3.0	41.1	32	40
4.2	1.6	57	9	زن	7 2-	3.2	36	34	4.	30	3 8	•	30	-	
								_				34		31.	4 ()
34	4.0	1.1	11.15	. 3	14.0	3.6	11 🛶	* O	40	56	11 14	41	76	4.5	۲.2
3.2	44	۶۶	<b>6</b> .	30	ς.	٠. (	ج ۱۰	40	۲۰.,	30	11 1	3 6	50	36	<b>5</b> )
	50	14	r. (1	-		-4.1	4, 3						-	-	
56		-		3 9				10	$a_{i,0}$	40	4 ~	• 11	110	. <b>;</b>	5.5
1.0	50	40	·• ,4	1)	c ,	41	٠,	45	ر ،	ાવ	۲,	44	50	44	<b>c</b> (,
44.11	50	1.4	<b>6</b> 5	40	6.2										
FINANCE	1.					, c			.,						
in Canada		F 1	CTFI					YEAR	7						
4/1	52	6. 16	42	. 4	c	4.4	r è	1.41	E 5	. , C	1. 6	4 1	۾ ر	3.5	E 6,
3,2	15	e \$	r >	3 1	15 6	3 6	τ, ,	ع تے	6 E	ê u	62	38	S p.	30	دن
		<u>1</u> 9												•-	-
34	60		4.4	<i>i</i>	F	1 b	7.5	i. 4	7 (⊹	22	* e:	è 4	<b>5€</b>	3 n	ė 8
36	54	<u> </u>	الريا	14.19	5 pi	ح ب		44	65.75	44	ti 💌	46	1.6	34	ű è
34	30	3 6	7.0	7.7	7 20	3.2	₹ 6	3/1	30	34	1.2	3:4	30	34	3.5
				-					-			-		_	_
3.4	40	3.6	1,	30	4.10	36	4. (*	3 ss	-7 ()	٠, (	1. 14	44 (	U 6.	40	114
3.6	46														
FINATCE		C. 5	CTETO	. 147		/ B C		YEAR	1						
			-				_								
3 r	e 4	3.0	٩.	34	'- C	311	3.6	34	l H	51.	16.2	7 .	36	34	₹ ⊱
31.	支持	34	2	٠,	ι,.	514	44	36	30	3.4	7.4	5+	41	ζA	4 2
	40	34	a +	ī ,	1.1	3.2	25	36				-			
5 ~		-							60	3.1	13/14	3 1	0.4	34	<b>3</b> 8
30	3 ()	30	11.77	3 1	5.0	۲ ز	40	30	ţ u	3.7	3.0	3 .	3.6	36	$v_{ij}$
3 ^	375	30	7,	۾ ج	7.5	2.0	4.6	2.8	ج ر.	cr	ام ،	17	1. 6	هج	<i>1: e</i>
-		ام تر				-						-			
ھ ح	16	<i>,</i> ~	3.4	è i	1 6	د ۽	t, $e$	٧ڔ	50	، خ	a o	i s	10 C	3 ^	46
3.3	13.0														
FIMALER		51 A	CTITO	1.45	)	/ P 🖰		YEAR	7						
					•							-			
32	40	32	1. 3	3 1		3 2	₹ (	32	117	' ?	3.6	.12	n c	3 n	F 14
11 >	4.85	40	F	43	£. ,	1 C.	40								
FIMANCE		٠.	1616	1 1 16		194		YEAR	7						
-	•														
n	30	٠	٠,	Ħ	1 ()	19	١¿	L/	16						
MARKET		٨ ٦	וו וויא בו	(r 125	i (4)	179		YEAR	7						
17	25	) //	7 :	12	ĩċ	15	72	10	20	12	ے ح	15	23	13	21
12	20	12	1 j.	۱۶	1.6	11	17	14	1 2.	15	1 3	1.0	1 8	A	1 8
Д	18	12	2 d	1 1	iř	12	21	1.1	19	G	2.5	۲	ں ج	16	2 n
16	24	14	2 6	12	3.5	۾`		Å	3.2		-			-	
							26			1.0	40	1,	40	10	, t. <sub>(*</sub>
4	34	r,	<b>7</b> 7	F	66	16	42	19	35	22	ام ح	19	ب ح	16	70
1.4	24	13	1.7	12	16	13	15					-		-	
MAPKET	•							V E A 7	,						
			-	[C 151				4 E M F	1						_
1 C	14	1/1	21.	12	<b>۱</b> ۲	16	2.8	10	3.3	14	<b>R</b> (4)	1 +	3 €	1 ^	3.:
16	32	18	20	1 8	٦٢	16	3 C	1/4	\$ 15	16	2 11	ī µ	24	17	25
								-				_		-	
17	21	16	22	1.5	20	12	<b>2</b> (	13	15	17	1 ~	10	16	G	15
۴	1 8	7	17	a	1 6	9	15	1 ()	10	¿1.	7 11	21	24	19	25
1 0	26	19	21	20	22	21	25	21	25					-	24
		· · · · · · · · · · · · · · · · · · ·								22	24	<i>2</i> 1	25	15	74
1 P	44	1 "	20	16	٠٠ ئم	16	76	14	10	14	ĉo	1.8	26		

MARKET		Δ	TEAST	Jr 12	7 1	1/79		YEAR	7						
14	26	14	د, و	13	21	12	74	A	, 5 a	Р	78	E	٠.	_	_
6	24	ρ	¿.,	10	22	5 v	2 %	16	56	16	55	5 16	31		28
10	14	Ç	+ 4	ŧσ	1 /-	12	نَع ﴿	12	1 11	10	20	10	2 U	17	10
7	23	16	10	15	3.7	16	20	• •		•	£ (	10	16	۴	20
MARKET		4	JLANT	10 12	A 1	1/79	, ,	YEAR	7						
1 ~	> 11	16	2.	1 5	19	12	26	12	18	12	16	Д	14	£	• .
٨	1 14	ľ	4 50	h	16	6	16	ρ	16	î,	13	10	نے آ	10	16
10	12	1 2	1 4	12	4.74	12	1 4	12	1 11	10	12	ja	1 -	1 *	14
1.0	16	12	10	1.0	10	11	15	14	18	•	-	•	• •	• •	~ 0
MARKET				10 12	9 11	1779		Y} Ah	7						
1 /4	2.0	12	2.2	1.3	ê c	ſυ	25	10	≥ ∨	10	20	12	20	12	18
1 0	1 6	( 2	> .	1 t	15	10	26	ρ	20	7	21	-	ء در	4	26
h	24	۴.	_ <b>&gt;</b> ^	,a	3 2	ρ.	5 ا	14	2.5	16	20	16	20		, 0
MARKET			-	10 13		179		YFAF	7						
10	55	11	21	17	3 8	16	26	18	26	18	25	19	21	4 1	20
12	1 A 1	10	14	1 1)	1.5	12	1 5	12	16	14	16	10	16	12	18
13	10	۲۶	1.4	12	1 0	15	16	1 0	5.7	10	20	1 4	10	12	14
12 Market	14		•											• -	• •
				11 13		779-0		YEAR	7						
12	14	13	ę ri	15	10	15	16	1/4	16	15	19	12	25	10	32
12	24	17	20	14	76	16	ي ح	14	2 ú	12	20	4	20	14	24
12	20	10	2.5	<i>k</i>	<i>हे</i> 0	1.0	2/1	1.0	20	12	2.5	1.2	26	Ā	28
1 0	28 28	10	21.	<i>+</i>	<u> </u>	4	3.4	5	76	4	34	1	35	4	34
MAPKET	~ ~		2	10	24	t	5 8	2	20	/1	30				٠.
2	3.4			Ir 13.		1790		YEAR	7						
		*	<b>t</b> /:	7	ž 4	۶	24	1 t	23	12	7 J	1.0	20	14	50
19 Market	ر) ح	16	21,	10 13											
25	<b>3</b> (:	10	* (2. 3 % ) . * (2. 1)			180	_		7						
56	24	5.0		1 0	26	2.4	26	24	26	24	26	55	20	20	24
14	24	مَرَ	، د د د	1 H 1 B	2 ÷ 28	24	3.0	4 نے	24	50	ĉ۶	20	25	18	26
2 0	26	1,0	72	-		0.5	بدخ	5.0	20	16	2.4	16	24	20	30
٨٤	30		16	l A	24	16	24	16	20	50	<b>∂</b> સ	22	ں ح	رږ	24
MARKET		٨	TIALT	IC 13/	1. 1. 3	780									
22	24	 خ خ	7.4	, 55 , 13,	د ۱۰ ۲۴	ر برج	30	AF V B	1		_				
د د	31	12	26	25	Ed	55		2.5	3.2	20	3.5	55	ろし	د ج	32
4	ςį	10	1ر 3	16	26	12	24 26	55	24	22	24	1 3	54	10	34
MARKET		-		[r 135			66	45 4 G	40	14	3.)	10	3 &	10	114
يه ج	3.2	2 4	7.1	أوج	1.4	3.0	32	32	34				_		
MARKET				tr 136		180	24		) <del>"</del>	54	36	24	38		
۾ ح	32	22	٦,	20	3.2	20	32	24	128	1.6	٠.				
"ARKET		۵.		to 137		183	٠.	YEAR		1.6	۶ ۲				
5.0	28	24	τ,	10	94.	16	44	10	5∵						
MARKET		4	TLAST	(1 138			•	YEAR							
4	44	۴	42	۾ .	2 %	16	36	25	30	20	2 4	, 4	٦.		•
ريا ح	ح ۶	ě li	رَة	27	31	26	ł c	يا ج	4.5	5.11		) E 24	26	1 4	56
يا ج	£ 44	24	<b>1</b> )	21.	Z 1,	28	3.0	24	26	65."-m.	10	۲.4	34	55	4 9
MARKET		Λ 1	[H] A (, T ]	11 137	L.F	180	. •	YFAR							
≥ a	26	<i>2</i> 0	ب <i>ر</i> ج	22	26	52	26	20	32	1 4	38	14	45	1 A	•
51	45	36	<b>3</b> .3	5.0	30	24	3.0	2 4	ŽЙ	25	28	, -		17	74
BESCI BC		Δ 1	たしゃくてき			179	-		7	- 1.	• 0				
30	\$4	ďη	₹ :1	54	36	64	۾ڄ	24	3.0	e. 4	32	22	30	25	34
24	34	24	¥ ct	50	38	24	42	52	0.2	22	4.3	36	46	30	
54	a H	S u	11 6	30	42	50	44	26	30	32	3.4	32	40	24	40
511	7 14	24	26	21	26	22	24	20	30	جَجَ	1.	18	3.	1 A	30
55	30	Ξn	3.5	50	26	25	24	22	24	65	24	2.5	76	50	28
50	10	20	17								` -	, .		£ ''	r n
PESCL PC			1 F VI 1 1			180		YEAR	7					,	
45	45	20	5.4	20	5.0	50	46	3.2	52	28	<b>5</b> 2	۾ڄ	46	55	64
54	45	ĉЬ	a n	5 11	۶.	26	52	2.5	56	211	چ	26	50	24	50
													-	-	-

5.4	48	20	44	12	70	10	ن ۾	16	52	16	5 U	20	5 U	12	58
1.0	58	5.5	ج>	26	(1.44	5 P	UC	AS	0.0	9.5	4 (	24	/le	24	46
èά	44	24	ua	22	4. É	52	4.4	26	45	36	u p	32	" c	32	34
32	36	34	6.4	34	66	40	1.6	311	42	34	E 14	36	Se	40	52
42	54	60	43.	žμ	1.4	36	10.44	4.0	یے با	3 11	40	57	56	2.0	40
ŤA.	40	36	4(1)	34	3.1	32	3.8	36	42	32	aэ	32	16	3.2	38
30	40	3.0	4.0	32	40	3 C	G Ç	26	30	٩ج	3.8	26	3 t	26	36
24	30	نا خ	3.6	24	15	26	36	20	36	24	30	24	36	26	34
26	34	ž e	72	24	3.2	2.8	36	28	36	2 P	34	î P	34	2 A	34
۾ خ	34	30	₹6	۾ڄ	40	2 🛱	64	3.0	4.4	2 P	44				
14 178 38		Λ.	161.7		) (u,	/ P ()		YEAR	7						
36	48	žИ	5 U	3 P	1.4	36	L P	36	56	36	ИĠ	3 P	34	36	38
45	30	24	₹6	4,2	36	32	36	3.0	3 4	26	3 %	211	3 e	2"	" 2
яç	45	20	15.0	20	l. F	20	t. P	) P	418	22	4 g	24	3€	5 b	3.6
a	34	32	70	24	<b>1</b> ()	30	3.8	3.2	40	3 U	36	32	31	32	3.6
30	36	32	иe	36	49,	36	o C	34	30	5 A	0.0	30	56	18	7 A
24	60	22	5,7	34	1: 31	38	45	30	34	30	32	2°	36	2 A	34
56	30	24	3 11	24	42										
RESCUR	CE	٨	TEART	10 9	\$ 6.4	-05/8	0	YEAR	1						
26	32	26	28	20	₹ (-	16	3.8	2.5	34	24	3.5	ہ نے	3 e	18	38
1 4	38	24	12	26	32	3 r	32	50	32	30	3.1	٩ς	34	32	36
37	30	32	16	54	4 C	34	38	36	38	32	42	2 "	44	24	44
۾ ج	44	۾ ح	8.0	28	4.0	30	36	2 A	34	28	3.5	26	32	24	34
2 /1	a 2	24	40	22	46	20	44	5.0	42	20	44	2 ۸	44	26	44
aج	0.0	5.6	76	2.8	7 -	58	4 C	32	44	34	44	34	Oc	35	44
3,2	40	34	46	40	12 12	3 P	116	3 A	4 0	36	6.4	36	46	36	44
36	42	īρ	11 17	36	1 6	36	42	36	44	36	4.4	26	3 c	30	1,4
RESITE	CE	٨	TI, At, T	Ic 3		/ H C		YEAR	7						
52	38	3.6	17	36	3.6	36	11.4	38	115	36	100	36	40	36	40
36	40	C ()	a c	32	3.4	3.0	3.4	۾ج	34	58	14	ĉч	3 e	211	3.5
7+	30	5.8	τι	2 F	\$ U	24	36	24	4.0	20	4.6	22	44	Σ'n	3.8
3,2	<b>ኛ</b> ሶ	3/4	4.8	7. P	1. 14	30	و (	3,2	5.0	36	40	34	44	36	11 0
34	42	3.0	46	32	4.5	3.0	48	36	46	36	3.6				
RESCUR	CF		TLAST	•		/ P ij		YEAR			_		-		
ی در	20	54	26	24	م ح	26	59	56	35	26	26	26	30	ĄĄ	32
3 r	44	30	14	3.0	3.4	30	3.4	30	36	30	3.9	32	# <b>(</b>	32	36
32	30	3/4	16	52	ą p	32	40	32	42	30	42	30	40	A is	36
5 4	36	32	4 F	37	3 13	٩ς	3.6	28	34	5 <sub>b</sub>	35	34	36	30	9.5

The Control of the Control

#### SHIP STRUCTURE COMMITTEE SL-7 REPORTS TO DATE

- SL-7-1, (SSC-238) Design and Installation of a Ship Response Instrumentation System Aboard the SL-7 Class Containership S.S. SEA-LAND MCLEAN by R. A. Fain. 1974. AD 780090.
  SL-7-2, (SSC-239) Wave Loads in a Model of the SL-7 Containership Running at Oblique Headings in Regular Waves by J. F. Dalzell and M. J. Chiocco. 1974. AD 780065.
  SL-7-3, (SSC-243) Structural Analysis of SL-7 Containership Under Combined Loading of Vertical,
- Lateral and Torsional Moments Using Finite Element Techniques by A. M. Elbatouti, D. Liu, and H. Y. Jan. 1974. AD-A002620.
- SL-7-4, (SSC-246) Theoretical Estimates of Wave Loads on the SL-7 Containership in Regular and Irregular Seas by P. Kaplan, T. P. Sargent, and J. Cilmi. 1974. AD-A004554.
- SL-7-5, (SSC-257) SL-7 Instrumentation Program Background and Research Plan by W. J. Siekierka, R. A. Johnson, and CDR C. S. Loosmore, USCG. 1976. AD-A021337.
- SL-7-6, (SSC-259) Verification of the Rigid Vinyl Modeling Techniques: The SL-7 Structure by J. L. Rodd. 1976. AD-A025717.
- SL-7-7, (SSC-263) Static Structural Calibration of Ship Response Instrumentation System Aboard the SEA-LAND MolEAN by R. R. Boentgen and J. W. Wheaton. 1976. AD-A031527.
- SL-7-8. (SSC-264) First Season Results from Ship Response Instrumentation Aboard the SL-7 Class Containership S.S. SEA-LAND MoLEAN in North Atlantic Service by R. R. Boentgen, R. A. Fain, and J. W. Wheaton. 1976. AD-A039752.
  SL-7-9, Second Season Results from Ship Response Instrumentation Aboard the SL-7 Class Container-
- ship S. S. SEA-LAND McLEAN in North Atlantic Service by J. W. Wheaton and R. R. Boentgen. 1976. AD-A034162.
- SL-7-10, Third Season Results from Ship Response Instrumentation Aboard the SL-7 Class Container-ship S. S. SEA-LAND MoLEAN in North Atlantic Service by R. R. Boentgen. 1976. AD-A034175. SL-7-11, (SSC-269) Structural Tests of SL-7 Ship Model by W. C. Webster and H. G. Payer. 1977.
- AD-A047117.
- SL-7-12,(SSC-271) A Correlation Study of SL-7 Containershit Loads and Motions Model Tests and Computer Simulation by P. Kaplan, T. P. Sargent, and M. Silbert. 1977. AD-A049349. SL-7-13, A Peront on Shipboard Waveheight Radar System by D. Chen and D. Hammond. 1978.
- AD-A053379.
- SL-7-14, (SSC-277) Original Radar and Standard Tucker Wavemeter SL-7 Containership Data Reduction and Correlation Samile by J. F. Dalzell. 1978. AD-A062394.
  SL-7-15, (SSC-278) Wavemeter Data Reduction Method and Initial Data for the SL-7 Containership
- by J. F. Dalzell. 1978. AD-A062391. SL-7-16, Radar and Tucker Wavemeter Data from S. S. SEA-LAND MoLEAN Voyage 30 by J. f. Dalzell. 1978. AD-A057154.
- SL-7-17, Radar and Tucker Waveneter Data from S. S. SEA-LANT Molean Voyage 33 by J. F. Dalzell. 1978. AD-A057155.
- SL-7-18, Radar and Tucker Wavemeter Data from S. S. SEA-LAND ModEAN Voyage 34 by J. F. Dalzell. 1978. AD-A057155.
- SL-7-19, Radar and Tucker Wavemeter Data from S. S. SEA-LAN: McLEAN Voyages 35 and 36E by J. F. Dalzell. 1978. AD-A057157.
- SL-7-20, (SSC-279) Modified Radar and Standard Tucker Wavemeter SL-7 Containership Data
- by J. F. Dalzell. 1978. AD-A062393.
  SL-7-21, Radar and Tucker Wavemeter Data from S. S. SEA-LAND MolEAN Voyage 66 by J. F. Dalzell. 1978. AD-A057004.
- SL-7-22, Radar and Tucker Wavemeter Data from S. S. SEA-LANT McLEAN Voyage 61 by J. F. Dalzell. 1978. AD-A057005.
- SL-7-23, (SSC-280) Results and Evaluation of the SL-7 Containership Radar and Tucker Wavemeter Data by J. F. Dalzell. 1978. AD-A062392.
- SL-7-24, (SSC-282) Comparison of Stresses Calculated Using the DAISY System to Those Measured on the SL-7 Containership Program by H-Y Jan, K-T Chang, and M. E. Wojnarowski. 1979. AD-A069031. SL-7-25, (SSC-286) - Results of the First Five "Data Years" of Extreme Stress Scratch.
- Gauge Data Collected Aboard SEA-LANI's SL-7's by R. A. Fain and E. T. Booth. 1979. AD-A072945.

- SL-7-26, (SSC-301) SL-7 Extreme Stress Data Collection and Reduction by E. T. Booth. 1981. SL-7-27, (SSC-311) Evaluation of SL-7 Scratch-Gauge Data by J. C. Oliver. 1981. SL-7-28, (SSC-313) SL-7 Research Program Summary, Conclusions and Recommendations by K. A. Stambaugh and W. A. Wood. 1981.

# SHIP RESEARCH COMMITTEE Maritime Transportation Research Board National Academy of Sciences - National Research Council

The SHIP RESEARCH COMMITTEE has technical cognizance of the interagency Ship Structure Committee's research program.

Mr. A. D. Haff, Chairman, Consultant, Annapolis, MD
Prof. A. H.-S. Ang, Civil Engrg. Dept., University of Illinois, Champaign, IL
Dr. K. A. Blenkarn, Research Director, Offshore Technology, Amoco Production
Company, Tulsa, OK

Mr. D. Price, Sr. Systems Analyst, National Oceanic and Atmospheric Administration, Rockville, MD

Mr. D. A. Sarno, Manager-Mechanics, ARMCO Inc., Middletown, OH Prof. H. E. Sheets, Dir. of Engineering, Analysis & Technology, Inc., Stonington, CT

Mr. J. E. Steele, Naval Architect, Quakertown, PA Mr. R. W. Rumke, Executive Secretary, Ship Research Committee

The SHIP DESIGN, RESPONSE, AND LOAD CRITERIA ADVISORY GROUP prepared the project prospectus and evaluated the proposals for this project.

Mr. J. E. Steele, Chairman, Naval Architect, Quakertown, PA

Mr. J. W. Boylston, Consulting Naval Architect, Giannotti & Associates, Inc., Annapolis, MD

Prof. R. G. Davis, Assistant Professor of Naval Architecture, Dept. of Marine Engrg., Texas A&M University, Galveston, TX

Mr. P. W. Marshall, Civil Engineering Advisor, Shell Oil Company, Houston, TX

Prof. R. Plunkett, Dept. of Aerospace Engrg. and Mechanics, University of Minnesota, Minneapolis, MN

Mr. C. B. Walburn, Assistant Naval Architect, Bethlehem Steel, Corp., Marine Division, Sparrows Point, MD

The SR-1245 ad hoc PROJECT ADVISORY COMMITTEE provided the liaison technical guidance, and reviewed the project reports with the investigator.

......

Mr. J. E. Steele, Chairman, Naval Architect, Quakertown, PA Mr. L. R. Glosten, L. R. Glosten Associates, Inc., Seattle, WA

Mr. P. M. Kimon, EXXON International Co., Florham Park, NJ

